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Static versus dynamic fracturing in shallow carbonate fault zones

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Title: Static versus dynamic fracturing in shallow carbonate fault zones

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Abstract: Moderate to large earthquakes often nucleate within and propagate through carbonates in the shallow crust. The occurrence of thick belts of low-strain fault-related breccias is relatively common within carbonate damage zones and was generally interpreted in relation to the quasi-static growth of faults. Here we report the occurrence of hundreds of meters thick belts of intensely fragmented dolostones along a major transpressive fault zone in the Italian Southern Alps. These fault rocks have been shattered in-situ with negligible shear strain accumulation. The conditions of in-situ shattering were investigated by deforming the host dolostones in uniaxial compression both under quasi-static (strain rate $\sim 10^{-5}$ s $^{-1}$) and dynamic (strain rate > 50 s $^{-1}$) loading. Dolostones deformed up to failure under low-strain rate were affected by single to multiple discrete extensional fractures sub-parallel to the loading direction. Dolostones deformed under high-strain rate were shattered above a strain rate threshold of ~ 120 s $^{-1}$ and peak stresses on average larger than the uniaxial compressive strength of the rock, whereas they were split in few fragments or remained macroscopically intact at lower strain rates. Fracture networks were investigated in three dimensions showing that low- and high-strain rate damage patterns (fracture intensity, aperture, orientation) were significantly different, with the latter being similar to that of natural in-situ shattered dolostones (i.e., comparable fragment size distributions). In-situ shattered dolostones were thus interpreted as the result of high energy dynamic fragmentation (dissipated strain energies > 1.8 MJ/m 3) similarly to pulverized rocks in crystalline lithologies. Given their seismic origin, the presence of in-situ shattered dolostones can be used in earthquake hazard studies as evidence of the propagation of seismic ruptures at shallow depths.

Manchester 15th August 2016

Dear Editor,

we would like the enclosed manuscript "**Static versus dynamic fracturing in shallow carbonate fault zones**" by M. Fondriest, M. - L. Doan, F. Aben, F. Fusseis, T. M. Mitchell, M. Voorn, M. Secco and G. Di Toro to be considered for publication in *Earth and Planetary Science Letters*.

In this study we investigated the origin (i.e., static versus dynamic) of ***in-situ shattered*** fault rocks within carbonate fault zones by combining field and microstructural observations (optical microscopy, scanning electron microscopy, X-ray microtomography) with rock deformation experiments (low strain rate uniaxial compression tests and high strain rate Split Hopkinson Pressure Bar tests).

The occurrence of thick belts of low-strain fault-related breccias is common within carbonate damage zones and was generally interpreted in relation to the quasi-static growth of faults (i.e., nucleation and interaction of various generations of joints, pressure solution seams and shear fractures) rather than to the propagation of earthquake ruptures. We recently reported the occurrence of hundreds of meters thick belts of intensely fragmented dolostones along a major transpressive fault zone in the Italian Southern Alps (Fondriest et al., *Tectonophysics*, 2015). Field and microstructural investigations supported the conclusion that these fault rocks were shattered *in-situ* with negligible shear strain accumulation.

In this new manuscript submitted to your attention, we demonstrated the seismic origin of the fragmented dolostones. We tested the mechanical behaviour of the dolomitic rocks in compression over a wide range of strain rates ($10^{-6} - 10^2 \text{ s}^{-1}$) to constrain the deformation conditions under which ***in-situ shattering*** occurs. We used image analysis techniques to discriminate between quasi-static and dynamic fracture patterns (i.e., 3D fracture pattern quantification, 2D fragment size distributions) and recognized ***in-situ shattering*** as a dynamic coseismic process (active at strain rates $> 120 \text{ s}^{-1}$). Experimentally shattered dolostones resembled well the natural ones (i.e., similar fragment size distributions) thus suggesting a common origin for the two.

In-situ shattered dolostones were thus interpreted as the result of high energy dynamic fragmentation (dissipated strain energies $> 1.8 \text{ MJ/m}^3$) in an equivalent way of pulverized rocks in crystalline lithologies, and can potentially be used as geological marker to assess the propagation of earthquake ruptures along carbonate fault zones at shallow depth.

The determination of both spatial distribution and fracture intensity of ***in-situ shattered*** fault rocks along seismogenic faults will help to better constrain the actual contribution of surface fracture energy in the earthquake energy budget and more

accurately determine the hazard related to seismogenic sources with incomplete earthquake catalogs.

Given the wide implications of this study, which can potentially appeal a large scientific community (from structural/earthquake geologists to rock mechanicians, seismologists and earthquake modelers), we think that our manuscript may be suitable for publication in *Earth and Planetary Science Letters*.

We confirm that this manuscript is not under consideration for other journals. We have included all our figures in colours, for which we have funding available should it be required.

On the behalf of the authors,

Michele Fondriest

Rebuttal letter of Fondriest et al., EPSL-S-16-01203

Author Responses to Reviewer Comments (responses in blue, boldface font)

We thank the Editor and the two Reviewers for their constructive and helpful comments. We addressed each main comment from the Reviewers individually and provide a point-by-point response below. Changes in text and figures with respect to the submitted version of the paper are pointed out.

More in detail, requests from both Reviewers (1 and 2) were carefully addressed by modifying the main text and some details of the figures (in addition Fig.7 and Fig.8 were swapped). To address the more substantial comments of Reviewer 1, two new subsections have been added to the main text: (1) subsection entitled "Fragment size distributions of the shattered dolostones" - "Result" section; (Lines 246-263 in the revised manuscript), and (2) subsection entitled "Shattered dolostones and hydraulic dilation breccias"- "Discussion and conclusions" section (Lines 310-334 in the revised manuscript). In these two subsections we explained carefully the way we determined and compared the fragments size distributions (FDS) of natural and experimental shattered dolostones, and ruled out the role of fluids in the formation of shattered dolostones of the Foiana Fault Zone by comparing the studied fault rocks with implosion hydraulic *crackle* breccias described in hydrothermal fault settings.

We hope that our replies will be satisfactory in order to get our manuscript published in your prestigious journal.

Best regards

Michele Fondriest, Mai-Linh Doan, Frans Aben, Florian Füsseis, Tom Mitchell, Maarten Voorn,
Michele Secco, Giulio Di Toro

Reviewer 1

(1) It is not clear from the paper if that shattering is exclusively related to dynamic impact. One factor that is overlooked in this study is the influence of pore fluid pressure, perhaps in the case of carbonates most likely CO₂. The "in-situ" shattering described here is similar to many examples of hydrothermal breccias formed by high pore fluid pressure. Neither interpretation of the field evidence or the experiments have allowed for this possibility. Dolostones show "in-situ" shattering remarkably commonly in the field. It may be that they are in all cases related to dynamic fracture, but the relationship of other dolostones to faults that could have been seismogenic remains to be demonstrated.

We understood the point of the Reviewer and carefully took it in consideration by adding a dedicated subsection entitled "Shattered dolostones and hydraulic dilation breccias" (Lines 310-334 in the revised version of the manuscript) to the "Discussion and conclusions" section. In this subsection we compare the textural characteristics of the shattered dolostones of the Foiana Fault Zone to those typically associated to implosion hydraulic breccias (sensu Sibson, 1986). Although both fault rocks can be described as *crackle* breccias (according to the non-genetic classification of Woodcock and Mort, 2008), the shattered dolostones described in our study do not contain veins

or large amounts of cement filling the fracture network (it is difficult to recognize cement even in thin sections), which are instead typical of implosion hydraulic (hydrothermal) breccias. In addition the structural setting is different too; indeed implosion breccias are associated to coseismically opening fault jogs, while in-situ shattered dolostones were reported both along straight fault segments and a big restraining fault bend (see Fig. 1a of this manuscript as well as Fondriest et. al, 2015). Moreover both quasi-static and dynamic loading experiments presented in our study were performed at “dry”-room humidity conditions and therefore did not consider the effect of pore fluid during fracturing. In this sense, the experiments we have performed were designed to investigate the origin of the fault rocks of the Foiana Fault Zone, that we interpreted to be produced during multiple coseismic stress wave loadings in a relatively fluid-poor environment.

(2) There is a problem with the terminology of "in-situ" to describe this fragmentation pattern. Literally, "in-situ" means that the rocks were in place when shattering occurred. All breccias start from this condition, and vary in the amount of subsequent displacement and fracturing of clasts. What is needed is a term that describes the fact that the clasts remain in the same place after shattering. There is a good description of such breccias by Woodcock and Mort: the term is jigsaw breccia.

We agree with the Reviewer comment and changed the manuscript accordingly. We described the shattered dolostones of the Foiana Fault Zone as *crackle* breccias, characterized by a well-fitted jigsaw puzzle texture (more than 75% of sample area covered by clasts > 2 mm in size) according to the non-genetic fault breccias classification of Woodcock and Mort (2008) (see Lines 311-317 in the revised version of the manuscript).

In relation to points (1) and (2) of the Reviewer we add the following references in the subsection “Shattered dolostones and hydraulic dilation breccias”:

Mitcham, T. W., 1974. Origin of breccia pipes, *Econ. Geol.*, 69, 412-413.

Phillips, W. J., 1972. Hydraulic fracturing and mineralization. *J. Geol. Soc. Lond.*, 128, 337-359.

Sibson, R. H., 1986. Brecciation processes in fault zones: inferences from earthquake rupturing, *Pure Appl. Geophys.*, 124, 159-175.

Tarasewicz, J. P. T., Woodcock, N. H., Dickson, J. A. D., 2005. Carbonate dilation breccias: examples from the damage zone to the Dent Fault, northwest England, *Geol. Soc. Am. Bull.*, 117, 736-745.

Woodcock, N. H., Omma, J. E., Dickson, J. A. D., 2006. Chaotic breccia along the Dent Fault, NW England: implosion or collapse of a fault void?, *J. Geol. Soc. Lond.*, 163, 431-446.

Woodcock, N. H., Mort, K., 2008. Classification of fault breccias and related fault rocks, *Geol. Mag.*, 145, 435-440.

(3) In general there are quite a few poorly written sentences, and use of unexplained jargon: non-hierarchical, high hierarchy and low hierarchy fracture patterns, and quasi-static are examples. Other problems are noted on the attached pdf. "i.e." is used unnecessarily and excessively. "Classic" is used (lines 78, 87, 277, 287), in a most inappropriate way: none of these results can be described as classic, so it is a confusing term. In some cases "classic" might be used in the sense of typical, but even the use of this word is problematic without adequate references to back up the generalization.

We agree with the Reviewer's comment and changed the text accordingly.

(4) Lines 87 - 90 imply that these papers specifically excluded dynamic fracturing: it is not clear that this is the case from these papers, even if they also refer to other mechanisms for creating breccias. It is also not clear enough if the details of the breccias described in these papers are similar to the subject of this paper. It might be better to raise this as a possibility, rather than making an all-out attack on the previous work.

We agree with the Reviewer's comment and decided to be more conservative in our statements. However, we wish to highlight that these studies did not exclude necessarily dynamic fracturing as a possible mechanism for grain fragmentation, but simply they did not consider or discuss it, since the papers were focused more on other fault zone growth models (mainly quasi-static). Anyway, our statements were not meant to be a criticism to these excellent previous studies and we apologize for the confusion we might have made.

(5) It might be useful to compare some of the experimental work with previous rock mechanic experiments on dolostone by Kennedy and coworkers: Austin et al. 2005 Textural controls on the brittle deformation of dolomite: the transition from brittle faulting to cataclastic flow. From: GAPAIS, D., BRUN, J. P. & COBBOLD, P. R. (eds) 2005. Deformation Mechanisms, Rheology and Tectonics: from Minerals to the Lithosphere. Geological Society, London, Special Publications, 243, 51-66.

We thank the Reviewer for highlighting this very interesting study. We carefully went through the manuscript of Austin et al. (2005) which performed triaxial tests at room temperature – room humidity conditions and confining pressures of 25 to 100 MPa on texturally different dolostones (low and high porosity ones). They investigated the transition from brittle faulting to cataclastic flow along discrete fractures produced in compression. The damage patterns are quite different from the ones described in our study, mainly due to the presence of confining pressure (up to an equivalent depth of ~ 4 km) and the application of small quasi-static strain rate, which inhibit fragmentation processes such as shattering and pulverization. Few similarities can be maybe recognized with the products of our quasi-static tests where a little amount of microscale shear deformation has been observed along the small internal (< 5 mm long) fractures.

Due to these substantial differences in the deformation patterns and in the scale at which the microstructural observations were performed [macroscopic fracture pattern in our case, and localized microscopic deformation in the case of Austin et al. (2005)], eventually we decided to not include the results of Austin et al. (2005) in the “Discussion and conclusions” section of our manuscript. Instead, we will consider this paper in our future studies which will be targeted on the evolution of fault zone damage with strain rate, temperature and confining pressure.

(6) There are very significant problems in comparing the fractal dimensions of the experimental fragments (0.73) with the measured breccias (1.1-1.2). In what way could these be called comparable? Why don't the values for the experiments (1.1. to 1.2) which are quoted in the text correspond to the numbers on Fig. 8B, and why are the latter not quoted in the text? Why choose those particular size ranges to measure the fractal dimension?

We completely understood the point raised by the Reviewer and recognized that the part of the manuscript about fragment size distributions (FSDs) was not clear enough. To address this important point, in the revised version of the manuscript we have widened the description of the

FSDs of natural shattered dolostones (Lines 127-135 in the revised manuscript) and added a new subsection entitled “Fragment size distributions of the shattered dolostones” in the “Results” section (Lines 246-263 in the revised manuscript) to compare the fragment size distributions of natural and experimental fault rocks. To do this we also have moved some parts of the text from the Supplementary Materials (as suggested elsewhere by the Reviewer) to the Main Text.

The main point in relation to the FSDs of shattered dolostones is that the size distributions can only be compared when determined on the same area (i.e., analysis domain). Therefore, as it is now explicitly stated in the revised text, the FSDs of natural shattered dolostones were determined in two dimensions on thin section scans (area $\sim 5 \text{ cm}^2$) which gave a representative view of the fault rock texture. The resulting curves in logarithmic plots are characterized by fragment size domains with different slopes; but if we exclude the lower and upper ranges of the fragment distributions which are clearly affected by undersampling effects, a linear trend with slopes of 1.2-1.3 can be recognized. It is clear from the curves shown in Fig.1f that it would be necessary to determine the distributions over a much larger fragment size range (up to three to four order of magnitude) to get a more complete and robust description of the FSDs of natural shattered dolostones, thus using measurements taken both at the hand sample and the SEM (high magnification images) scale. However this topic requires a dedicated study. For this reason, in the main text, we never refer to fractal dimensions (but only about slopes of the curves in the logarithmic plots), since it was not possible to define a distribution fractal (i.e., self-similar) on the limited investigated fragment size ranges (up to two orders of magnitudes at maximum). Since the FSDs of the experimental samples were determined on smaller analysis domains (area $\sim 0.8 \text{ cm}^2$) which were constrained by the dimensions of the tested samples, the FSDs of natural shattered dolostones were then recalculated on the same analysis domain of $\sim 0.8 \text{ cm}^2$ to allow us a comparison. The resulting FSDs have comparable trends (see Fig.7) with average slopes of ~ 0.7 in the size range 0.1-1 mm. Clearly the slopes determined on these areas are smaller compared to those shown in Fig.1f mainly due to undersampling effects, but maybe also because the distributions might be neither self-similar nor spatially homogeneous. Again these last two statements are only hypotheses that require to be verified through a dedicated analysis. Our aim in this study was only to compare the fragment size distributions of natural and experimental shattered dolostones on the available size ranges (limited by the dimensions of the tested samples and by the resolutions of the X-ray tomographic images).

In more detail:

For the natural samples:

1. Why was this particular range chosen to measure the fractal dimensions?
2. This is very far from the range for which the straight line is shown in Fig. 1.
3. Over this range of size, there is not a straight line on the cumulative plots.
4. It should be stated in the text (not just the supplementary material) that these are 2D values.

We agree with the Reviewer and answered to all these points (1-4) in the paragraph above. We also made the following changes to the manuscript:

- (i) widening of the description of FSDs in natural shattered dolostones (Lines 246-263 in the revised manuscript),

- (ii) writing a new subsection entitled “Fragment size distributions of the shattered dolostones” in the “Results” section (Lines 246-263 in the revised manuscript) of the manuscript.

For the experiments:

1. Why is the size range over which the fractal dimension is measured different from the previous size range used for the natural samples?
2. The lines are fitted for a considerably smaller size range than stated for individual examples

We agree with the Reviewer and answered to all these points (1-2) in the paragraph above. We also made the following changes to the manuscript:

- (i) widening of the description of FSDs in natural shattered dolostones (Lines 246-263 in the revised manuscript),
- (ii) writing a new subsection entitled “Fragment size distributions of the shattered dolostones” in the “Results” section (Lines 246-263 in the revised manuscript) of the manuscript.

From the data in Fig. 8, it does indeed seem as though the experimental and natural samples have comparable size distributions over limited ranges. However, a rule of thumb for a valid fractal dimension is that it should be determined over an order of magnitude variation in size, so focussing on these apparently arbitrary size ranges for making the comparisons is not the best analysis.

We agree with the Reviewer about the limit of using a small size range in the analysis, but this is basically due to the limited dimensions of the experimental samples. Moreover we never refer to fractal dimensions or self-similarity of the measured fragment size distributions.

Finally, on the particle size distributions, it is clear that they are being used to make a comparison, but it would be better if they were also compared to dynamic fragmentation values in the literature, which are surprisingly higher.

As the Reviewer correctly stated, in our study the FSDs are only used to make a comparison between natural and experimental shattered rocks on the same limited analysis domain (area ~ 0.8 cm²). For these reasons and all the limitations described above we did not compare our results with published “fractal” dimensions of natural pulverized rocks and experimental samples derived from high-strain rate experiments (e.g., impact tests, explosions). However, it is evident that the FSDs of the shattered dolostones described in our study are different from those of the pulverized rocks, which are clearly more fine-grained on average.

(7) The paper is very well backed up with supplementary data, almost too excess, so that some important aspects of the supplementary data should be in the text.

We followed the suggestion of the Reviewer and moved some text from the Supplementary Material to the Main Text, in particular in the section about fragment size distributions (see main answer to point 6 of the Reviewer above).

All the other minor corrections and improvements to the text proposed by the Reviewer (both in the review letter and the annotated .pdf file) were included in the revised version of the manuscript.

Reviewer 2

Moderate comments:

(1) Lines 232-235: "Experimental results indicate that intensely fragmented in-situ shattered dolostones were produced in compression when the applied critical strain rate was $> 120 \text{ s}^{-1}$ and the peak stress was larger than the uniaxial compressive strength of the rock ($227.3 \pm 45 \text{ MPa}$) (Figs. 4a-c)." I'm not sure I agree: for highest critical strain rates the peak axial stress linearly decreases (even below the UCS). Therefore rocks are shattered even at relatively low peak axial stress. I think that the authors should make it clear and discuss this point.

We understood the very good point raised by the Reviewer. Anyway, based on both on the quasi-static and dynamic loading experiments we performed, it is quite clear that the tested dolostones were characterized by a large variability of the mechanical parameters (see for example the wide standard deviation associated to the uniaxial compressive strength – UCS values in Fig.2a). This is likely due to the textural heterogeneity (i.e., grain size and *facies* variations) typical of natural dolostones. Therefore we discussed the comment of the Reviewer by modifying a couple of sentences (Lines 204-206 in the revised manuscript), and stating that in-situ shattering occurred when the applied peak stress was on average larger than the uniaxial compressive strength of the rock. Moreover the possibility that the dynamic compressive strength of the rock (which should be larger compared to the quasi-static UCS) decreases with increasing strain rate is difficult to be physically justified (i.e., rock strength and elastic moduli usually increase with increasing strain rates).

(2) The discussion is in general clear and discussing the main results. However I would recommend the authors to add a subsection that compare and discuss the relations between on-fault and off-fault indicators for seismic slip. The principal author of this paper did an excellent and extensive study of the Foiana fault and shows the results of tens of rock experiments in this manuscript and in his two previous papers (published in 2013 and 2015). This is one of the studies that have the best records of both on and off fault observations that are supported with the results of lab experiments. One of the main questions that is still open and especially for carbonate rocks is regarding the indicator for seismic slip. The author reported about mirror like surfaces in Foiana fault in his 2013 paper and suggested that they may form during seismic slip. This paper suggests that seismic activity pulverized the fault zone rocks. I think it is very important to discuss both and to suggest what we know and what is still needed to be explored in that sense.

We appreciated the comment of the Reviewer and we agree that it is fundamental to gain a more unified view of what we know about off- and on-fault coseismic processes in carbonate rocks. Therefore we followed the suggestion of the Reviewer and briefly described the presence of highly localized mirror-like fault surfaces (Lines 329-334 in the revised manuscript) cutting through

shattered dolostones of the Foiana Fault Zone (these features were largely investigated in previously published studies by some of the authors). The presence of mirror-like faults sharply truncating clasts of the host dolostones was interpreted as an evidence of coseismic shear strain localization (Fondriest et al., 2013, 2015) and may therefore reinforce the inference of a dynamic origin of the shattered dolostones too.

Minor comments:

Line 1: In the title you use the word "Static" although in the manuscript you use "quasi-static" is there any difference? Please be more precise about it and define clearly the terms quasi-static and dynamic in the introduction (I'm not sure that the short explanation in the abstract is enough, lines 31-32). I would explain these terms before lines 53-55.

We understand the comment of the Reviewer. There is no difference between the terms static and quasi-static in the use we did.

Line 156-157: "Quasi-static uniaxial compression tests were performed on both jacketed and unjacketed samples...". Is there any difference in results between the jacketed and unjacketed samples? I don't think it was mentioned or discussed along the manuscript and it may be an interesting point (or not).

This is a good question of the Reviewer. We did not observe any clear difference in the mechanical behaviour of jacketed and unjacketed samples. Therefore we considered that the confinement effect due to the plastic jacket was negligible.

Lines 158-160 and Fig. 2a: I wonder, what is the point of plotting the strength versus the size ratio? I would plot it versus the volume to show size effect, i.e. the effect of sample size on strength.

According to our experience it is quite normal to plot uniaxial compressive strength of the rock vs. length to diameter ratio of the samples (see Mogi, 1966, 2007; Paterson and Wong, 2005).

Mogi, K., 1966. Some precise measurements of the fracture strength of rocks under uniform compressive stress, *Felsmechanik und Ingenieurgeologie*, 4, 41-55.

Mogi, K., 2007. *Experimental rock mechanics*, Taylor & Francis, London, p. 361.

Paterson, M. S., Wong, T.-F., 2005. *Experimental rock deformation – the brittle field*, Springer-Verlag.

Line 188-190: "Samples loaded at critical strain rates $> 120 \text{ s}^{-1}$ and peak stresses of $> 200 \text{ MPa}$ (over the average UCS limit, Figs. 4a, b) accumulated residual strains $> 2\%$ (Figs. 3c, d) and were typically intensely fragmented (Fig. 3c)". But there are also shattered rocks that were formed under peak stress $< 200 \text{ MPa}$. See also my first moderate comment.

Please, see our reply to the first moderate point of the Reviewer.

Lines 481-482: Did you look at the nano-scale? Is the crystal size minimum limit is a real physical effect or a resolution effect of your observations?

This is a very good point of the Reviewer. We did not have the chance to carefully look at the nano-scale (few hundreds of nanometers) well below the sizes of the crystals. We clearly saw the presence of angular fragments of few micrometers in size, but it can be that also those fragments were affected by incipient fragmentation and fracturing looking at a finest scale.

Lines 495-496: "(number of voxels with a given orientation; see Voorn et al., 2015)". I'm not sure I understand, is it the poles to each fracture surfaces? I would make this point clearer.

Following Voorn et al. (2015) the pole figures represent the three dimensional orientation information of each voxel belonging to fractured which have been previously segmented through the use of the Multiscale Hessian Fracture Filter – MSHFF defined in Voorn et al., 2013. We changed the sentence “number of voxels with a given orientation” in the figure caption to “poles to fracture planes” as it is written in Voorn et al. (2015).

All the other minor comments (including typos corrections) and suggestions of the Reviewer were taken in consideration and the text was modified accordingly to them.

All the modifications performed in the revised version of the manuscript are highlighted in blue.

Static versus dynamic fracturing in shallow carbonate fault zones

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Keywords: in-situ shattering, dynamic loading, earthquakes, quasi-static loading, carbonates, fractures

23

24 **ABSTRACT**

25 Moderate to large earthquakes often nucleate within and propagate through carbonates in the
26 shallow crust. The occurrence of thick belts of low-strain fault-related breccias is relatively
27 common within carbonate damage zones and was generally interpreted in relation to the quasi-
28 static growth of faults. Here we report the occurrence of hundreds of meters thick belts of
29 intensely fragmented dolostones along a major transpressive fault zone in the Italian Southern
30 Alps. These fault rocks have been shattered *in-situ* with negligible shear strain accumulation.
31 The conditions of *in-situ* shattering were investigated by deforming the host dolostones in
32 uniaxial compression both under quasi-static (strain rate $\sim 10^{-5} \text{ s}^{-1}$) and dynamic (strain rate $>$
33 50 s^{-1}) loading. Dolostones deformed up to failure under low-strain rate were affected by single
34 to multiple discrete extensional fractures sub-parallel to the loading direction. Dolostones
35 deformed under high-strain rate were shattered above a strain rate threshold of $\sim 120 \text{ s}^{-1}$ and
36 peak stresses on average larger than the uniaxial compressive strength of the rock, whereas
37 they were split in few fragments or remained macroscopically intact at lower strain rates.
38 Fracture networks were investigated in three dimensions showing that low- and high-strain
39 rate damage patterns (fracture intensity, aperture, orientation) were significantly different,
40 with the latter being similar to that of natural *in-situ* shattered dolostones (i.e., comparable
41 fragment size distributions). *In-situ* shattered dolostones were thus interpreted as the result of
42 high energy dynamic fragmentation (dissipated strain energies $> 1.8 \text{ MJ/m}^3$) similarly to
43 pulverized rocks in crystalline lithologies. Given their seismic origin, the presence of *in-situ*

shattered dolostones can be used in earthquake hazard studies as evidence of the propagation of seismic ruptures at shallow depths.

1. INTRODUCTION

Unstable fracture propagation and fragmentation are fundamental processes dominating brittle deformation of solid materials loaded upon and beyond their elastic limit (e.g., Scholz, 2002). The mechanics of fracturing is strongly controlled by the loading configuration (tensile or compressive) since in tension a single crack can grow unstably (i.e., accelerating) until sample failure, whereas in compression a population of small cracks propagates stably (i.e., steady growth rate) until stress interaction leads to instability and sample failure (Ashby and Sammis, 1990). Fracture growth rates can range from stable quasi-static low velocities to dynamic ones comparable or higher than the Rayleigh wave velocity of the host material (e.g., Freund, 1990).

These considerations are particularly relevant when applied to rocks and fault zones in which fractures are widespread. Experimental deformation of both rocks and analogue materials (e.g., polymer composites) investigated the spectrum of propagation rates, from stable to dynamic, for growing shear and tensile single fractures nucleated under various loading configurations. As a result two major features, namely high angle tensile fractures and macro- to micro branching were recognized to be exclusively associated to dynamic fracture propagation (e.g., Sagy et al., 2001; Griffith et al., 2009; Fineberg et al., 1991, 1999). High angle tensile fractures compare well with off-fault injection veins which are currently considered as clear evidence of earthquake ruptures in the field, especially when filled with pseudotachylites

or fluidized fault rocks (Di Toro et al., 2005; Rowe and Griffith, 2015). Conversely this is not the case for branching fractures which can even be induced by quasi-static loading (Sagy et al., 2004). This means that besides investigating the growth velocity of single fractures, it is important to determine the loading conditions (e.g. loading and strain rates) responsible for the production of certain fracture patterns both in experiments and in nature.

The characterization of rock damage and the identification of dynamic signatures within fault zones have fundamental implications for earthquake mechanics and in particular for the constraint of energy budgets involved in seismic fracturing (e.g., Shipton et al., 2006; Pittarello et al., 2008). To date rock pulverization (i.e., fragmentation down to the crystal size scale with no shear strain accommodation) is the only large-scale macroscopic feature clearly relatable to dynamic off-fault damage induced during the propagation of earthquake ruptures. Indeed pulverized rocks have been reported in tens to hundreds of meters thick bands along major faults (Dor et al., 2006, Mitchell et al., 2011) and were produced in the laboratory under high strain rate loading conditions (Doan and Gary, 2009; Yuan et al., 2011). Fine-grained pulverized rocks (sensu Brune et al., 2001) seem to be exclusively formed at shallow depth (less than 3 km) within homogeneous stiff protoliths (mainly granitoids) while their occurrence was not frequently reported for heterogeneous sedimentary covers. The latter is the case for carbonates (i.e., limestones and dolostones), which are worldwide distributed lithologies dominating the upper crust of many seismically active regions where moderate to large magnitude earthquakes occur (e.g., 2008 Wenchuan Mw 7.9 and 2009 L'Aquila Mw 6.1 earthquakes; Burchfiel et al., 2008; Chiarabba et al., 2009). In particular, the occurrence of thick belts (10-100s m) of low-strain, poorly distorted breccias (average size of rock fragments > 1

cm) is common within carbonate fault zones of various kinematics exhumed from a few kilometers (e.g., Billi et al., 2003). These damage patterns were frequently interpreted in relation to the quasi-static growth of fault zones characterized by the sequential formation and activation of joints, pressure solution seams, veins, shear fractures during prolonged polyphasic deformations (e.g., Salvini et al., 1999; Billi et al., 2003; Agosta et al., 2006).

Here we investigate the alternative possibility that some of these fragmented rocks in carbonate fault zones may have a coseismic dynamic origin. We report the occurrence of thick belts of *in-situ* shattered dolostones along a major transpressive fault zone in the Italian Southern Alps and test the mechanical behavior of the dolomitic host rocks in compression over a wide range of strain rates ($10^{-6} - 10^2 \text{ s}^{-1}$) to constrain the deformation conditions under which *in-situ* shattering occurs. We used image analysis techniques to discriminate between quasi-static and dynamic fracture patterns and inferred *in-situ* shattering as a dynamic coseismic process. We finally consider the implications of our experimental results for the mechanics of earthquakes and the scaling relationships of fault zones in carbonates.

2. IN-SITU SHATTERED DOLOSTONES OF THE FOIANA FAULT ZONE

The Foiana Fault Zone is a ~30 km long major sinistral transpressive fault exhumed from < 2 km depth in the Italian Southern Alps. The fault zone crosscuts Permo-Triassic igneous and sedimentary rocks, the latter including thick sequences of dolostones, with cumulative vertical throw of 0.3-1.8 km (Fig. 1a) (Prosser, 1998). The host rock (Mendola Formation – peritidal member) consists of light-gray sedimentary dolostones with cycles up to 0.6–1 m thick characterized by stromatolitic laminations and planar trails of *fenestrae* (Avanzini et al., 2001;

Fondriest et al., 2015). The crystal size is in the range 20-300 μm , with the larger crystals filling diagenetic pores (see Fondriest et al., 2015 for full description). Measured acoustic/elastic properties of the host dolostones are: $V_p = 6.54 \pm 0.46 \text{ km/s}$, $V_s = 3.64 \pm 0.15 \text{ km/s}$, dynamic Young modulus = $94.04 \pm 9.04 \text{ GPa}$, while total Helium porosity is $1.7 \pm 0.8 \%$ (see Supplementary Material).

The fault zone is exposed within badland areas and consists of > 300 m thick belts of intensely fractured and fragmented dolostones which have been shattered *in-situ* with negligible shear strain accumulation (Fig. 1b, see Fondriest et al., 2015). This is documented by the preservation of primary sedimentary features (i.e., bedding surfaces, marly dolostone horizons and stromatolitic laminations; see inset in Fig. 1b) even in the most highly fragmented rock bodies. At the outcrop scale dolostones are reduced into fragments ranging from few centimeters down to few millimeters in size separated by joints and extensional micro-fractures. Joints are fault-related and are arranged in different sets (the most pervasive sets are parallel and perpendicular to fault strike; rose diagrams in Fig. 1a) displaying complex cross-cutting/abutting relations (Figs. 1a, b). At the meso- to micro-scale these rocks are affected by a pervasive and non-hierarchical fracture pattern with variable fracture orientations, locally resulting in the development of micro-fragmentation zones (fracture spacing < 1 mm) (Figs. 1c-e). Fragment size distributions (FSD) (also named clast size distributions – CSD) measured in two dimensions by manual drawing on thin section scans (area $\sim 5 \text{ cm}^2$) cover a clast size range of 0.05-7 mm with average slopes of 1.2-1.3 in logarithmic plots (Figs. 1e-f) (see Supplementary Materials for details). The slopes were computed in the narrower range of 0.4-2 mm where the curves had a linear trend (Fig. 7), thus avoiding the external intervals. In fact, the latter are affected by bias

related to the spatial resolution of the images (data truncation) and to the finite size of the analysis domain (data censoring). The clast size distributions determined on fault parallel and fault perpendicular orientations were comparable (Fig.1f).

3. METHODS

To understand the origin of the *in-situ* shattered dolostones of the Foiana Fault Zone low- to high- strain rate uniaxial compression experiments were performed on rock cylinders cored from the Mendola Formation. Low-strain rate ($\sim 10^{-5} \text{ s}^{-1}$) tests were performed with a uniaxial hydraulic test apparatus at the Rock and Ice Physics Laboratory at University College London and a uniaxial hydraulic press at the Geoscience Department rock deformation laboratory in Padova. High-strain rate ($> 50 \text{ s}^{-1}$) tests were conducted with a mini-Split Hopkinson Pressure Bar (SHPB) at the ISTerre laboratory in Grenoble (Aben et al., 2016a). Quasi-static uniaxial tests (N=16) were run both in displacement and stress control mode on 20 and 25 mm in diameter rock cylinders with various length/diameter ratios (~ 1 -2.4) (Table 1). Dynamic SHPB tests (N=29) were run on samples with length/diameter ratio ~ 1 to reduce inertia effects (Gama et al., 2004; Zhang and Zhao, 2014) and diameters of 10, 15 and 20 mm to explore a wide range of peak stresses and strain rates (Table 1). Applied strain (i.e., loading duration) was controlled by changing the length of the steel striker bar while striker impact velocity was kept fixed around 5 m/s. Cardboard pulse shapers were used to guarantee stress equilibrium conditions during the tests. Further details on the different apparatuses are summarized in Supplementary Material.

Some of the samples were wrapped with a heat-shrinkable plastic jacket to be recovered after the experiments (both quasi-static and dynamic loading tests) and analyze the produced fracture pattern. Deformed samples were impregnated with epoxy and petrographic thin sections cut both perpendicular and approximately parallel to the loading direction were prepared for microstructural observations [optical microscopy (OM) and scanning electron microscopy (SEM)]. Three dimensional fracture patterns were described through image analysis techniques (software: FIJI, CTAn) applied to X-ray scan datasets acquired at different spatial resolutions ($8 \times 8 \times 8 \mu\text{m}^3$ and $23 \times 23 \times 23 \mu\text{m}^3$ per voxel), while fragment size distribution (FSD) was determined in two dimensions both for natural and experimental shattered rocks (see Supplementary Material for details).

4. RESULTS

4.1. MECHANICAL DATA AND DAMAGE STATES

Quasi-static uniaxial compression tests were performed on both jacketed and unjacketed samples with varying length to diameter ratio at strain rates of $6.7 \times 10^{-6} \text{ s}^{-1}$ and $6.7 \times 10^{-5} \text{ s}^{-1}$. Measured uniaxial strengths (UCS) and static Young moduli (average values: $227.3 \pm 45 \text{ MPa}$ and $64.1 \pm 18 \text{ GPa}$ respectively, see Supplementary Material) were relatively scattered and did not show any correlation with either strain rate or sample geometry (Fig. 2a). The observed variability was likely a consequence of the mechanical heterogeneity of the tested rock. Samples loaded up to failure accumulated permanent axial strains of 0.2-0.7% while elastic strain energy ($E_{diss-\sigma MAX}$ in Table 1, calculated as the area below the “axial stress vs. axial strain” curve) dissipated up to the peak stress was $0.4\text{-}1 \text{ MJ/m}^3$. The common failure mode was

longitudinal “sub-axial” splitting (*sensu* Holzhausen and Johnson, 1979) with fractures oriented parallel or at small angle ($<10^\circ$) to the loading direction and cutting through the entire sample. Many of these fractures were concentrated in the outer portion of the sample, where radial expansion is expected to be higher, and had a curvilinear trace in plain view (exfoliation extensional fractures) (Figs. 2b, c). Instead, the central portion of the sample consisted of a continuous "pillar" affected by short (<5 mm trace length) closed shear fractures and staircase arrays of oblique fractures and sub-axial wing cracks (Figs. 2b, c). In some cases the development of a through going Andersonian-oriented leading shear fracture (i.e., sample faulting) was observed (inset in Fig. 2a).

Dynamic SHPB tests performed on both jacketed and unjacketed samples spanned peak stresses of 60-360 MPa, axial strains of 0.3-3% and peak strain rates of $140\text{-}450\text{ s}^{-1}$ (Table 1, Figs. 3-4). The stress, strain and strain rate histories of the dynamically loaded samples highlight the applied peak stress and the critical strain rate (ϵ'_c in Table 1) as primary factors in controlling the mechanical behavior and the ultimate damage state of the samples. As previously observed by Aben et al. (2016a) the critical strain rate ϵ'_c represents the plateau or inflection point value of the strain rate vs. time curve and roughly matches in time with the applied peak stress (Figs. 3a,b). When recovered after loading the samples were (i) macroscopically intact (Fig. 3a), (ii) split in few pieces (Fig. 3b), or (iii) intensely fragmented (Fig. 3c). Samples loaded at critical strain rates of $\sim 20\text{ s}^{-1}$ and peak stresses of 100-150 MPa (below the average UCS limit, Figs. 4a, b) showed a quasi-elastic stress-strain behavior (residual strains $\sim 0.2\%$, Figs. 3a, d) and were macroscopically intact or split if they contained preexisting heterogeneities (e.g., sub-axial veins, Fig. 3a). Samples loaded at critical strain rates $\sim 50\text{ s}^{-1}$ and

peak stresses ≤ 200 MPa (around the average UCS limit, Figs. 4a, b) accumulated residual strains of 0.4-0.6% (Figs. 3b, d) and were split or macroscopically intact (Fig.3b). Samples loaded at critical strain rates $> 120 \text{ s}^{-1}$ and peak stresses of ≥ 200 MPa (around and over the average UCS limit, Figs. 4a, b) accumulated residual strains $> 2\%$ (Figs. 3c, d) and were typically intensely fragmented (Fig. 3c). In this case the strain rate at which fragmentation occurred was a relative minimum in the strain rate vs. time curve, preceding a second strain rate peak occurring during sample unloading (Aben et al., 2016a) (Fig.3c). Dissipated strain energy during fragmentation was in the range 1.5-2.8 MJ/m³ (E_{diss} in Table 1), almost 30% of the kinetic energy transferred by the striker impact to the steel bar (E_{kin} in Table 1, calculated as $E_{kin} = 0.5 \times m \times v^2$, where m is the striker mass and v the striker impact velocity; Fig. 4c). These samples were reduced into a non-cohesive material with angular rock fragments mostly of few millimeters in size (Fig. 3c). Looking at *in-situ* microstructures (X-ray tomography and microscopy on thin sections), the fragments were elongated in the loading direction and delimited by subparallel extensional fractures crosscut by a few orthogonal ones (Figs. 5a, b). Diffuse tensile microfracturing exploiting both cleavage planes and grain boundaries occurred along the main fractures and at the side where the stress wave entered the sample (Figs. 5c, d). Such microstructures, coupled with the general absence of shear strain, are very similar in natural *in-situ* shattered dolostones (compare Figs. 5a, d with Figs. 1c-e).

4.2. FRACTURE PATTERN ANALYSIS

The three-dimensional fracture patterns of quasi-statically and dynamically deformed samples were quantified and compared by using image analysis applied to X-ray computed tomography datasets (for details see Supplementary Material) (Figs. 6a-c). To extract the

fracture network from the tomographic images we used the approach implemented by Voorn et al. (2013) (multiscale Hessian fracture filter – MSHFF) for the software FIJI (Schindelin et al., 2012), which was optimized for the enhancement and segmentation of narrow planar features such as fractures (see Supplementary Material). Further properties of the fracture network such as fracture intensity, bulk fracture orientation and aperture were determined after Voorn et al. (2015) using both FIJI and CTAn software (for details see Supplementary Material). The fracture skeletons were analyzed in two dimensions on slices oriented orthogonal to the loading direction.

Volumetric fracture intensity values (total fracture surface/sample volume) were significantly higher for dynamically shattered samples ($\sim 4.0 \text{ mm}^{-1}$) compared to quasi-statically fractured ones ($\sim 1.4 \text{ mm}^{-1}$) (Fig. 6b). Bulk fracture aperture followed a unimodal distribution (modal value $\sim 0.03 \text{ mm}$ for samples S4 and S26, Fig. 6c) in shattered samples while it was characterized by a polymodal distribution (modal values $> 0.1 \text{ mm}$ for sample U4, Fig. 6c) in quasi-statically fractured samples. In both cases fractures were oriented almost parallel to the loading direction (Fig. 6b). In terms of strike fractures generated under dynamic loading were quite scattered or arranged in a orthorhombic geometry (“low hierarchy” fracture pattern), while fractures produced under quasi-static loading were clustered around the orientation of few leading fractures (“high hierarchy” fracture pattern) (Figs. 6a, b). Overall the fracture patterns produced by dynamic loading were characterized by a much higher number of fracture branches and intersections compared to the quasi-static ones (Fig. 6d).

4.3. FRAGMENT SIZE DISTRIBUTIONS OF THE SHATTERED DOLOSTONES

Fragment size distributions (FSD) of experimental shattered dolostones were determined in two dimensions by manual drawing on X-ray tomographic images over an area of $\sim 0.8 \text{ cm}^2$ which was constrained by the dimensions of the experimental samples (for details see Supplementary Material). To allow a comparison, the FSDs of natural shattered dolostones (see Fig.1f) were recalculated on the same smaller analysis domains (area $\sim 0.8 \text{ cm}^2$) (Fig.7). The resulting FDSs of both natural and experimental shattered dolostones were comparable in the size range 0.01-4 mm with an average slope of 0.73 ± 0.14 in logarithmic plots (Fig.7). The slopes were computed in the narrower range of 0.1-1 mm where the curves had a linear trend (Fig.7), thus avoiding the external intervals which are affected by bias related to the spatial resolution of the images (data truncation) and to the finite size of the analysis domain (data censoring). Recalculated slopes (D) of natural shattered dolostones are smaller (~ 0.7 on average; Fig.7) than the ones determined on larger analysis domains (~ 1.2 on average; Fig.1f). The different slopes in the fragment distributions plots are certainly due to the undersampling effects associated to the reduction of the analysed sampled area. However, the diverse slopes might also suggest that the FSDs of these rocks are neither spatial heterogeneous nor self-similar. To investigate this hypothesis it would be necessary to determine the fragment size distributions over a much larger size range (i.e. three to four orders of magnitude).

5. DISCUSSION AND CONCLUSIONS

5.1. ENERGY SINKS AND DAMAGE

Experimental results indicate that intensely fragmented *in-situ* shattered dolostones were produced in compression when the applied critical strain rate was $> 120 \text{ s}^{-1}$ and the peak stress was on average larger than the uniaxial compressive strength of the rock (227.3 ± 45

MPa) (Figs. 4a-c). In particular, when we considered the strain energy dissipated in the sample up to the peak stress ($E_{diss-\sigma MAX}$ in Table 1), the occurrence of an energy threshold of ~ 1.8 MJ/m³, above which *in-situ* shattering start to develop, was evident (Fig.8). Interestingly this energy threshold was larger than the total energy dissipated in the pulverization of crystalline rocks such as quartz-monzonite (~ 1.5 MJ/m³; Aben et al., 2016a) and calcitic marble (~ 1.1 MJ/m³; Doan and Billi, 2011). Estimates of surface fracture energies for the shattered samples (E_s in Table 1) were 40-80% of dissipated strain energy (E_{diss} in Table 1, see Supplementary Material). The dynamically fragmented samples had distinctive characteristics compared to quasi-statically fractured ones: (i) higher fracture intensity, (ii) narrower fractures, (iii) low-hierarchy and high-complexity of the fracture pattern (Figs. 6a-d). All these characteristics are consistent with high strain rate loading during which the energy supply to the sample is too fast to be dissipated by only few fractures: this results in intense fragmentation of the rock (Grady and Kipp, 1989; Bhat et al., 2012; Doan and d'Hour, 2012, Aben et al, 2016b). On the other hand quasi-statically loaded samples displayed typical low-rate propagation features such as subaxial wing cracks growing at the tips of inclined fractures (e.g., Ashby and Sammis, 1990). Instead, the relatively abundance of curvilinear fractures in the outer portion of the samples was due to non-uniform stress distribution and lack of confinement during the tests (Peng and Johnson, 1972), and has to be considered as an artifact when compared with natural fault rocks. This was not the case for dynamically loaded samples, which were instead affected by radial fractures due to the occurrence of dynamic confinement (radial confinement up to ~ 0.5 MPa, see Supplementary Material) at high loading rates, when the effect of material inertia becomes significant (Doan and Gary, 2009; Chen, 2011).

5.2. IN-SITU SHATTERING: NATURE VS. LAB

In-situ shattered dolostones were exclusively produced at high dynamic loading rates in the laboratory. The deformation conditions determined for shattering in dolostones (critical strain rate $> 120 \text{ s}^{-1}$, axial strain $> 2\%$, Fig. 4) were comparable to those associated to pulverization of homogeneous crystalline rocks (i.e., granite, quartz-monzonite, calcitic marble; Doan and Gary, 2009; Yuan et al., 2011, Doan and Billi, 2011; Aben et al., 2016a) and considered to be transiently achieved in the fault wall rocks during the propagation of an earthquake rupture (e.g., Ben-Zion and Shi, 2005; Reches and Dewers, 2005). Moreover, in contrast to the quasi-statically deformed samples, experimentally shattered dolostones showed striking similarities with the natural ones of the Foiana Fault Zone: (i) two dimensional FSDs determined at the scale of the experimental samples (area $\sim 0.8 \text{ cm}^2$) were comparable (average slope = 0.73 ± 0.14 , size range = $0.01\text{-}4 \text{ mm}$) (Figs. 7), (ii) rock fragments were frequently exploded with no evidence of shear strain, (iii) pervasive extensional fracturing locally occurred down to the micrometer scale (microfragmentation domains) (Figs. 1c-e and Figs. 5a-d). All these observations suggest that also natural *in-situ* shattered dolostones had a dynamic origin potentially related to multiple off-fault coseismic stress-wave loadings (Fondriest et al., 2015).

5.3 SHATTERED DOLOSTONES AND HYDRAULIC DILATION BRECCIAS

The shattered dolostones of the Foiana Fault Zone are characterized by a well-fitted jigsaw puzzle texture which in most of the cases is comparable to that of the *crackle breccias* defined by Woodcock and Mort (2008) in their “non-genetic” fault breccias classification (more than 75% of sample area covered by clasts $> 2 \text{ mm}$ in size). This type of fault breccia was originally described in the dolomitic host rocks of the Dent Fault (northwest England) and

characterized by extensive infill of the fracture network by hydrothermal carbonate cement (Tarasewicz et al., 2005; Woodcock et al., 2006). In a similar way many *crackle* and *shatter* breccias described in the mining literature as fault-related were associated to hydraulic implosion mechanisms and frequently cemented by the deposition of hydrothermal minerals (e.g., Phillips, 1972; Mitcham, 1974; Sibson, 1986). According to Sibson (1986) implosive brecciation is a dynamic coseismic process generated by a sudden collapse of the wall rock at dilational fault jogs (mainly during rupture arrest) coupled with the generation of strong pore fluid pressure gradients. Compared to implosion hydraulic breccias, the shattered dolostones of the Foiana Fault Zone (i) were observed in different fault zone sections (straight fault segments and restraining bends; Fig. 1a) and, (ii) did not show presence of veins or cement filling the fracture network (see Fondriest et al., 2015 for details). Basing on the experimental results presented in this study (all the experiments were performed in “dry”- room humidity conditions, see section 3) *in-situ* shattered dolostones of the Foiana Fault Zone are the result of off-fault coseismic damage due to the propagation of multiple earthquake ruptures in a relative fluid-poor environment. This hypothesis might be furtherly reinforced by the occurrence of other structural features such as highly localized mirror-like fault surfaces lined by thin ultracataclastic layers, sharply truncating the shattered dolostones and previously interpreted as evidence of extreme coseismic shear strain localization based on field, microstructural and experimental observations (see for more details Fondriest et al., 2013, 2015).

5.4. IMPLICATIONS FOR SCALING RELATIONS IN FAULT ZONES

The experimental observations presented [here](#) open the possibility to reinterpret the origin of low-strain breccias (10-100s m thick) frequently associated with fault zones in

328 carbonates and classically interpreted in relation to the “slow” quasi-static growth of faults (i.e.,
329 nucleation and interaction of various generations of joints, pressure solution seams and shear
330 fractures; e.g., Salvini et al., 1999; Billi et al., 2003; Agosta et al., 2006). Many of these breccias,
331 especially within stiff dolomitic protoliths, might instead be produced by dynamic shattering
332 during the propagation of earthquake ruptures and then be more efficiently affected by
333 dissolution-precipitation and mass transfer processes during the post- or inter-seismic periods
334 (e.g., Gratier et al. 2014). Following this line of thought most of the volume of these fault zones
335 would be generated during earthquakes as it is also suggested by aftershocks spatial
336 distributions along active seismogenic faults (e.g., Valoroso et al., 2013). Moreover faults
337 associated with *in-situ* shattered fault rocks are frequently characterized by thickness vs.
338 displacement (t/d) ratios which are significantly higher (i.e., $t/d \sim 1$) compared to the classical
339 scaling relations estimated for relatively “simpler” fault zones (i.e., characterized by discrete
340 fault surfaces and well described by the “*damage zone-fault core*” model of Caine et al., 2010)
341 according to purely geometric quasi-static growth models ($t/d \sim 0.1$; e.g., Childs et al., 2009).
342 This is particularly evident within near-tip fault sections, as in the case of the southern sector of
343 the Foiana Fault Zone, where cumulative displacement tends to be low and the effects of slip
344 accumulation by stable sliding are likely to be minimized (Fig. 9). Therefore the occurrence of
345 high thickness vs. displacement ratios, coupled with the presence of *in-situ* shattered fault
346 rocks, can potentially be used to assess (i) the propagation of earthquake ruptures at shallow
347 depth along carbonate fault zones, and (ii) the hazard related to seismogenic sources with
348 incomplete earthquake catalogs. As a consequence the accurate mapping of the distribution of
349 *in-situ* shattered fault rocks along seismogenic fault zones and the precise quantification of

their fracture intensity represent the base for future robust evaluations of the actual contribution of surface fracture energy in the earthquake energy balance at shallow depth (i.e., < 3 km).

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Figure 1. Natural *in-situ* shattered fault rocks. (a) Aerial view of the central and southern sectors of the Foiana Fault Zone (Southern Alps, Italy; see inset on the top right): main fault strands colored in red. Actual and inferred exposures of *in-situ* shattered dolostones along fault strike were represented by blue areas; attitudes of the bedding around the fault were indicated with white symbols. Low-hemisphere projection stereoplots represent joints attitude (both as poles to planes and strike rose diagrams) moving from south (outcrop 1) to north (outcrop 2) along fault strike. Joints were mainly parallel and perpendicular to the average fault strike. (b) View of the Foiana Fault Zone (outcrop 1) exposed within a badland area. The exposed fault zone is > 300 m thick and consists of *in-situ* shattered rocks: intensely fragmented dolostones with little to no evidence of shear strain (see inset on the right). (c-e) Rock fragments of the *in-situ* shattered dolostones ranged from few centimeters down to few millimeters in size (c: hand specimen photograph; e: tracings of the clasts at the thin section scale) and (d) were locally

characterized by micro-fragmentation zones affected by penetrative extensional fracturing down to the micrometer scale. (f) Clast size distribution of *in-situ* shattered dolostones measured at the thin section scale (investigated area $\sim 5 \text{ cm}^2$) in directions both parallel and perpendicular to the fault strike. The two distributions had comparable slopes in the cumulative number (N) vs. equivalent diameter logarithmic plot.

Table 1. List of uniaxial compression tests of this study. High-strain rate uniaxial compression tests (#test: S1-S29) and low-strain rate uniaxial compression tests (#test: U1-U18). Symbols: d = sample diameter; L = sample length; σ_{MAX} = peak axial stress; UCS = uniaxial compressive strength; ϵ_{AMAX} = maximum axial strain; ϵ_{R} = residual axial strain; ϵ'_{MAX} = maximum strain rate; ϵ'_A = applied strain rate; ϵ'_C = critical strain rate; E_{KIN} = input kinetic energy; E_{diss} = dissipated strain energy; $E_{\text{diss-}\sigma\text{MAX}}$ = dissipated strain energy up to the peak stress; E_s = surface fracture energy; damage = sample damage state after the test. Damage: I = macroscopically intact; sp = split; SH = shattered; F = incipient and prominent fragmentation; f = sample faulted; sp+f = sample split and faulted. Indications: gages broken = strain gages broken during the test.

Figure 2. Low strain rate uniaxial compression tests. (a) Relation between uniaxial compressive strength (UCS) and length to diameter ratio of the Mendola Formation rock cylinders tested at strain rates of 6.7×10^{-6} and $6.7 \times 10^{-5} \text{ s}^{-1}$. UCS values were relatively scattered. In the photo, macroscopic Andersonian-oriented fracture of a sample at the end of experiment U12. (b) Thin section scan of the fractured sample U2 cut parallel to the loading direction (indicated by the vertical black arrow). The sample was affected by sub-axial extensional fractures (longitudinal

splitting) more densely concentrated in the outer portion of the sample. The internal portion of the sample U2 was affected by staircase arrays of oblique fractures (red in colour) and sub-axial wing-like cracks. (c) Thin section scan of the fractured sample U2 cut perpendicular to the loading direction. The sample was affected both by circular and radial extensional fractures in its outer portion and tiny closed shear fractures associated to shear comminution within the inner portion (see magnified SEM-BSE image in the inset).

Figure 3. High strain rate uniaxial compression tests. (a-c) Axial stress (blue in color line), axial strain (red line) and strain rate (green line) histories of dynamically loaded samples and associated damage states. σ_{MAX} and ϵ'_c indicate the peak axial stress and critical strain rate respectively, following the terminology of Table 1. Shattered samples (Fig. 3c) were characterized by a peculiar mechanical history compared to macroscopically intact and split ones, with a double-pick strain rate path. The relative strain rate minimum corresponds to the critical strain rate value for shattering in the test. (d) Stress vs. axial strain history of dynamically loaded samples. Macroscopically intact and split samples showed a quasi-elastic to anelastic behavior with residual strains <1%. Shattered samples accumulated residual strains always > 2%.

Figure 4. Deformation conditions for *in-situ* shattering. (a-c) Summary of high strain rate compression experiments. Samples were shattered over strain rates of $\sim 120 \text{ s}^{-1}$ if the applied peak stress was on average higher than the average UCS of the rock. Moreover experimentally

shattered samples showed a distinct clustering compared to the other samples in terms strain energy dissipation.

Figure 5. *In-situ* microstructures of experimentally shattered samples. (a) X-ray microtomography slice (sample S4) oriented perpendicular to the loading direction. Intense rock fragmentation with fine-grained material (down to the micrometer scale) lining main fractures is recognizable. Stress (blue line), strain (red line) and strain rate (green line) history of sample S4 is reported in the top left inset. (b) SEM-BSE images mosaic of the shattered sample S4 cut parallel to the loading direction (black in color arrow). Rock fragments were mostly few millimeters in size, elongated in the loading direction and delimited by sub-parallel extensional fractures. Pulverization (extensional fracturing down to the micrometer/crystal size scale) occurred along the main fractures (some of the infilling material was lost during sample polishing) and at the side where the stress wave entered the sample (see BSE-SEM magnified image in the inset). (c-d) SEM-BSE images with details of rock pulverization by crystal boundary breakage and fragmentation along cleavage planes.

Figure 6. Fracture pattern analysis. (a) X-ray tomography slices of the fracture pattern of a quasi-statically fractured sample (test U4) and a dynamically shattered one (test S26) enhanced by the application of a multiscale Hessian fracture filter (MSHFF) (Voorn et al., 2013). Since quasi-statically loaded samples were larger compared to dynamically shattered ones, which were even affected by dynamic confinement effects, both the entire (e.g., U4 in the figure) and inner-core (e.g. U4sub in the figure) fracture pattern of quasi-statically fractured samples were

compared with dynamically shattered ones. The yellow dashed circumference delimits U4sub which is comparable in size to sample S26 (the size comparison is highlighted by the two yellow dashed lines). (b) Three dimensional fractures orientation ([poles to fracture planes](#); see Voorn et al., 2015). Quasi-statically fractured samples (test U4) were affected by few circular fractures and many Andersonian-oriented leading fractures (high hierarchy pattern). Dynamically shattered samples (test S26) were affected by many fractures with variable strike orientation and few leading ones (low hierarchy pattern). Volumetric fracture intensity was always larger for dynamically shattered samples compared to quasi-statically fractured ones. (c) Three dimensional fracture aperture distribution (number of voxel per aperture interval) was significantly different (polymodal vs. unimodal) for quasi-static fractured samples compared to dynamically shattered ones. (d) The two dimensional fracture skeleton of dynamically shattered samples was characterized by a higher number of fracture branches compared to quasi-statically fractured ones.

Figure 7. Two dimensional fragment size distribution of (i) natural *in-situ* shattered dolostones measured on sections oriented both parallel and perpendicular to the average strike of the Foiana Fault Zone, and (ii) experimental shattered dolostones measured on sections oriented perpendicular to the loading direction. The distributions of both natural and experimental samples were comparable (i.e. similar slopes), thus suggesting a common dynamic origin for these shattered rocks. The clast size distributions were measured on equivalent surfaces of 0.78 cm^2 which was constrained by the dimension of the experimental samples.

Figure 8. Plot of dissipated strain energy up to the peak stress vs. maximum axial strain. Experimentally shattered samples were characterized by much higher axial strains and slightly higher strain energies dissipated up to the peak stress compared to the quasi-statically fractured ones. Peculiarly shattered samples were produced only when an energy threshold of $\sim 1.8 \text{ MJ/m}^3$ was overcome, which was significantly higher compared to the energy dissipated by quasi-static compressive fracturing.

Figure 9. Fault rocks thickness vs. cumulative fault displacement scaling relations after Childs et al. (2009) for various host rocks and fault kinematics (a,b). *In-situ* shattered dolostones at the southern portion of the Foiana Fault Zone (displacement = 0.3-0.5 km, outcrop 1 in Fig.1a) were > 300 m thick and lied out of the scaling trend displayed in the plots which are associated to quasi-static fault growth models. Moving to the north (outcrop 2 in Fig.1a) the cumulative displacement increased up to 1.6-1.8 km and the thickness of shattered rocks was $\sim 100 \text{ m}$. Here the scaling relation was more consistent with the one proposed by Childs et al. (2009).

Highlights

In-situ shattering is the result of high-energy dynamic rock fragmentation.

Quasi-static and dynamic fracture patterns are significantly different.

Experimental in-situ shattered dolostones resemble the natural ones.

In-situ shattered dolostones are geological markers of earthquake ruptures.

Static versus dynamic fracturing in shallow carbonate fault zones

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23

24 **ABSTRACT**

25 Moderate to large earthquakes often nucleate within and propagate through carbonates in the
26 shallow crust. The occurrence of thick belts of low-strain fault-related breccias is relatively
27 common within carbonate damage zones and was generally interpreted in relation to the quasi-
28 static growth of faults. Here we report the occurrence of hundreds of meters thick belts of
29 intensely fragmented dolostones along a major transpressive fault zone in the Italian Southern
30 Alps. These fault rocks have been shattered *in-situ* with negligible shear strain accumulation.
31 The conditions of *in-situ* shattering were investigated by deforming the host dolostones in
32 uniaxial compression both under quasi-static (strain rate $\sim 10^{-5} \text{ s}^{-1}$) and dynamic (strain rate $>$
33 50 s^{-1}) loading. Dolostones deformed up to failure under low-strain rate were affected by single
34 to multiple discrete extensional fractures sub-parallel to the loading direction. Dolostones
35 deformed under high-strain rate were shattered above a strain rate threshold of $\sim 120 \text{ s}^{-1}$ and
36 peak stresses on average larger than the uniaxial compressive strength of the rock, whereas
37 they were split in few fragments or remained macroscopically intact at lower strain rates.
38 Fracture networks were investigated in three dimensions showing that low- and high-strain
39 rate damage patterns (fracture intensity, aperture, orientation) were significantly different,
40 with the latter being similar to that of natural *in-situ* shattered dolostones (i.e., comparable
41 fragment size distributions). *In-situ* shattered dolostones were thus interpreted as the result of
42 high energy dynamic fragmentation (dissipated strain energies $> 1.8 \text{ MJ/m}^3$) similarly to
43 pulverized rocks in crystalline lithologies. Given their seismic origin, the presence of *in-situ*

shattered dolostones can be used in earthquake hazard studies as evidence of the propagation of seismic ruptures at shallow depths.

1. INTRODUCTION

Unstable fracture propagation and fragmentation are fundamental processes dominating brittle deformation of solid materials loaded upon and beyond their elastic limit (e.g., Scholz, 2002). The mechanics of fracturing is strongly controlled by the loading configuration (tensile or compressive) since in tension a single crack can grow unstably (i.e., accelerating) until sample failure, whereas in compression a population of small cracks propagates stably (i.e., steady growth rate) until stress interaction leads to instability and sample failure (Ashby and Sammis, 1990). Fracture growth rates can range from stable quasi-static low velocities to dynamic ones comparable or higher than the Rayleigh wave velocity of the host material (e.g., Freund, 1990).

These considerations are particularly relevant when applied to rocks and fault zones in which fractures are widespread. Experimental deformation of both rocks and analogue materials (e.g., polymer composites) investigated the spectrum of propagation rates, from stable to dynamic, for growing shear and tensile single fractures nucleated under various loading configurations. As a result two major features, namely high angle tensile fractures and macro- to micro branching were recognized to be exclusively associated to dynamic fracture propagation (e.g., Sagy et al., 2001; Griffith et al., 2009; Fineberg et al., 1991, 1999). High angle tensile fractures compare well with off-fault injection veins which are currently considered as clear evidence of earthquake ruptures in the field, especially when filled with pseudotachylites

or fluidized fault rocks (Di Toro et al., 2005; Rowe and Griffith, 2015). Conversely this is not the case for branching fractures which can even be induced by quasi-static loading (Sagy et al., 2004). This means that besides investigating the growth velocity of single fractures, it is important to determine the loading conditions (e.g. loading and strain rates) responsible for the production of certain fracture patterns both in experiments and in nature.

The characterization of rock damage and the identification of dynamic signatures within fault zones have fundamental implications for earthquake mechanics and in particular for the constraint of energy budgets involved in seismic fracturing (e.g., Shipton et al., 2006; Pittarello et al., 2008). To date rock pulverization (i.e., fragmentation down to the crystal size scale with no shear strain accommodation) is the only large-scale macroscopic feature clearly relatable to dynamic off-fault damage induced during the propagation of earthquake ruptures. Indeed pulverized rocks have been reported in tens to hundreds of meters thick bands along major faults (Dor et al., 2006, Mitchell et al., 2011) and were produced in the laboratory under high strain rate loading conditions (Doan and Gary, 2009; Yuan et al., 2011). Fine-grained pulverized rocks (*sensu* Brune et al., 2001) seem to be exclusively formed at shallow depth (less than 3 km) within homogeneous stiff protoliths (mainly granitoids) while their occurrence was not frequently reported for heterogeneous sedimentary covers. The latter is the case for carbonates (i.e., limestones and dolostones), which are worldwide distributed lithologies dominating the upper crust of many seismically active regions where moderate to large magnitude earthquakes occur (e.g., 2008 Wenchuan Mw 7.9 and 2009 L'Aquila Mw 6.1 earthquakes; Burchfiel et al., 2008; Chiarabba et al., 2009). In particular, the occurrence of thick belts (10-100s m) of low-strain, poorly distorted breccias (average size of rock fragments > 1

cm) is common within carbonate fault zones of various kinematics exhumed from a few kilometers (e.g., Billi et al., 2003). These damage patterns were frequently interpreted in relation to the quasi-static growth of fault zones characterized by the sequential formation and activation of joints, pressure solution seams, veins, shear fractures during prolonged polyphasic deformations (e.g., Salvini et al., 1999; Billi et al., 2003; Agosta et al., 2006).

Here we investigate the alternative possibility that some of these fragmented rocks in carbonate fault zones may have a coseismic dynamic origin. We report the occurrence of thick belts of *in-situ* shattered dolostones along a major transpressive fault zone in the Italian Southern Alps and test the mechanical behavior of the dolomitic host rocks in compression over a wide range of strain rates ($10^{-6} - 10^2 \text{ s}^{-1}$) to constrain the deformation conditions under which *in-situ* shattering occurs. We used image analysis techniques to discriminate between quasi-static and dynamic fracture patterns and inferred *in-situ* shattering as a dynamic coseismic process. We finally consider the implications of our experimental results for the mechanics of earthquakes and the scaling relationships of fault zones in carbonates.

2. IN-SITU SHATTERED DOLOSTONES OF THE FOIANA FAULT ZONE

The Foiana Fault Zone is a ~30 km long major sinistral transpressive fault exhumed from < 2 km depth in the Italian Southern Alps. The fault zone crosscuts Permo-Triassic igneous and sedimentary rocks, the latter including thick sequences of dolostones, with cumulative vertical throw of 0.3-1.8 km (Fig. 1a) (Prosser, 1998). The host rock (Mendola Formation – peritidal member) consists of light-gray sedimentary dolostones with cycles up to 0.6–1 m thick characterized by stromatolitic laminations and planar trails of *fenestrae* (Avanzini et al., 2001;

110 Fondriest et al., 2015). The crystal size is in the range 20-300 μm , with the larger crystals filling
111 diagenetic pores (see Fondriest et al., 2015 for full description). Measured acoustic/elastic
112 properties of the host dolostones are: $V_p = 6.54 \pm 0.46 \text{ km/s}$, $V_s = 3.64 \pm 0.15 \text{ km/s}$, dynamic
113 Young modulus = $94.04 \pm 9.04 \text{ GPa}$, while total Helium porosity is $1.7 \pm 0.8 \%$ (see
114 Supplementary Material).

115 The fault zone is exposed within badland areas and consists of > 300 m thick belts of intensely
116 fractured and fragmented dolostones which have been shattered *in-situ* with negligible shear
117 strain accumulation (Fig. 1b, see Fondriest et al., 2015). This is documented by the preservation
118 of primary sedimentary features (i.e., bedding surfaces, marly dolostone horizons and
119 stromatolitic laminations; see inset in Fig. 1b) even in the most highly fragmented rock bodies.
120 At the outcrop scale dolostones are reduced into fragments ranging from few centimeters
121 down to few millimeters in size separated by joints and extensional micro-fractures. Joints are
122 fault-related and are arranged in different sets (the most pervasive sets are parallel and
123 perpendicular to fault strike; rose diagrams in Fig. 1a) displaying complex cross-cutting/abutting
124 relations (Figs. 1a, b). At the meso- to micro-scale these rocks are affected by a pervasive and
125 non-hierarchical fracture pattern with variable fracture orientations, locally resulting in the
126 development of micro-fragmentation zones (fracture spacing < 1 mm) (Figs. 1c-e). Fragment
127 size distributions (FSD) (also named clast size distributions – CSD) measured in two dimensions
128 by manual drawing on thin section scans (area $\sim 5 \text{ cm}^2$) cover a clast size range of 0.05-7 mm
129 with average slopes of 1.2-1.3 in logarithmic plots (Figs. 1e-f) (see Supplementary Materials for
130 details). The slopes were computed in the narrower range of 0.4-2 mm where the curves had a
131 linear trend (Fig. 7), thus avoiding the external intervals. In fact, the latter are affected by bias

related to the spatial resolution of the images (data truncation) and to the finite size of the analysis domain (data censoring). The clast size distributions determined on fault parallel and fault perpendicular orientations were comparable (Fig.1f).

3. METHODS

To understand the origin of the *in-situ* shattered dolostones of the Foiana Fault Zone low- to high- strain rate uniaxial compression experiments were performed on rock cylinders cored from the Mendola Formation. Low-strain rate ($\sim 10^{-5} \text{ s}^{-1}$) tests were performed with a uniaxial hydraulic test apparatus at the Rock and Ice Physics Laboratory at University College London and a uniaxial hydraulic press at the Geoscience Department rock deformation laboratory in Padova. High-strain rate ($> 50 \text{ s}^{-1}$) tests were conducted with a mini-Split Hopkinson Pressure Bar (SHPB) at the ISTerre laboratory in Grenoble (Aben et al., 2016a). Quasi-static uniaxial tests (N=16) were run both in displacement and stress control mode on 20 and 25 mm in diameter rock cylinders with various length/diameter ratios (~ 1 -2.4) (Table 1). Dynamic SHPB tests (N=29) were run on samples with length/diameter ratio ~ 1 to reduce inertia effects (Gama et al., 2004; Zhang and Zhao, 2014) and diameters of 10, 15 and 20 mm to explore a wide range of peak stresses and strain rates (Table 1). Applied strain (i.e., loading duration) was controlled by changing the length of the steel striker bar while striker impact velocity was kept fixed around 5 m/s. Cardboard pulse shapers were used to guarantee stress equilibrium conditions during the tests. Further details on the different apparatuses are summarized in Supplementary Material.

Some of the samples were wrapped with a heat-shrinkable plastic jacket to be recovered after the experiments (both quasi-static and dynamic loading tests) and analyze the produced fracture pattern. Deformed samples were impregnated with epoxy and petrographic thin sections cut both perpendicular and approximately parallel to the loading direction were prepared for microstructural observations [optical microscopy (OM) and scanning electron microscopy (SEM)]. Three dimensional fracture patterns were described through image analysis techniques (software: FIJI, CTAn) applied to X-ray scan datasets acquired at different spatial resolutions ($8 \times 8 \times 8 \mu\text{m}^3$ and $23 \times 23 \times 23 \mu\text{m}^3$ per voxel), while fragment size distribution (FSD) was determined in two dimensions both for natural and experimental shattered rocks (see Supplementary Material for details).

4. RESULTS

4.1. MECHANICAL DATA AND DAMAGE STATES

Quasi-static uniaxial compression tests were performed on both jacketed and unjacketed samples with varying length to diameter ratio at strain rates of $6.7 \times 10^{-6} \text{ s}^{-1}$ and $6.7 \times 10^{-5} \text{ s}^{-1}$. Measured uniaxial strengths (UCS) and static Young moduli (average values: $227.3 \pm 45 \text{ MPa}$ and $64.1 \pm 18 \text{ GPa}$ respectively, see Supplementary Material) were relatively scattered and did not show any correlation with either strain rate or sample geometry (Fig. 2a). The observed variability was likely a consequence of the mechanical heterogeneity of the tested rock. Samples loaded up to failure accumulated permanent axial strains of 0.2-0.7% while elastic strain energy ($E_{diss-\sigma MAX}$ in Table 1, calculated as the area below the “axial stress vs. axial strain” curve) dissipated up to the peak stress was $0.4\text{-}1 \text{ MJ/m}^3$. The common failure mode was

longitudinal “sub-axial” splitting (*sensu* Holzhausen and Johnson, 1979) with fractures oriented parallel or at small angle ($<10^\circ$) to the loading direction and cutting through the entire sample. Many of these fractures were concentrated in the outer portion of the sample, where radial expansion is expected to be higher, and had a curvilinear trace in plain view (exfoliation extensional fractures) (Figs. 2b, c). Instead, the central portion of the sample consisted of a continuous “pillar” affected by short (<5 mm trace length) closed shear fractures and staircase arrays of oblique fractures and sub-axial wing cracks (Figs. 2b, c). In some cases the development of a through going Andersonian-oriented leading shear fracture (i.e., sample faulting) was observed (inset in Fig. 2a).

Dynamic SHPB tests performed on both jacketed and unjacketed samples spanned peak stresses of 60-360 MPa, axial strains of 0.3-3% and peak strain rates of $140\text{--}450\text{ s}^{-1}$ (Table 1, Figs. 3-4). The stress, strain and strain rate histories of the dynamically loaded samples highlight the applied peak stress and the critical strain rate (ϵ'_c in Table 1) as primary factors in controlling the mechanical behavior and the ultimate damage state of the samples. As previously observed by Aben et al. (2016a) the critical strain rate ϵ'_c represents the plateau or inflection point value of the strain rate vs. time curve and roughly matches in time with the applied peak stress (Figs. 3a,b). When recovered after loading the samples were (i) macroscopically intact (Fig. 3a), (ii) split in few pieces (Fig. 3b), or (iii) intensely fragmented (Fig. 3c). Samples loaded at critical strain rates of $\sim 20\text{ s}^{-1}$ and peak stresses of 100-150 MPa (below the average UCS limit, Figs. 4a, b) showed a quasi-elastic stress-strain behavior (residual strains $\sim 0.2\%$, Figs. 3a, d) and were macroscopically intact or split if they contained preexisting heterogeneities (e.g., sub-axial veins, Fig. 3a). Samples loaded at critical strain rates $\sim 50\text{ s}^{-1}$ and

peak stresses ≤ 200 MPa (around the average UCS limit, Figs. 4a, b) accumulated residual strains of 0.4-0.6% (Figs. 3b, d) and were split or macroscopically intact (Fig. 3b). Samples loaded at critical strain rates $> 120 \text{ s}^{-1}$ and peak stresses of ≥ 200 MPa (around and over the average UCS limit, Figs. 4a, b) accumulated residual strains $> 2\%$ (Figs. 3c, d) and were typically intensely fragmented (Fig. 3c). In this case the strain rate at which fragmentation occurred was a relative minimum in the strain rate vs. time curve, preceding a second strain rate peak occurring during sample unloading (Aben et al., 2016a) (Fig. 3c). Dissipated strain energy during fragmentation was in the range 1.5-2.8 MJ/m³ (E_{diss} in Table 1), almost 30% of the kinetic energy transferred by the striker impact to the steel bar (E_{kin} in Table 1, calculated as $E_{kin} = 0.5 \times m \times v^2$, where m is the striker mass and v the striker impact velocity; Fig. 4c). These samples were reduced into a non-cohesive material with angular rock fragments mostly of few millimeters in size (Fig. 3c). Looking at *in-situ* microstructures (X-ray tomography and microscopy on thin sections), the fragments were elongated in the loading direction and delimited by subparallel extensional fractures crosscut by a few orthogonal ones (Figs. 5a, b). Diffuse tensile microfracturing exploiting both cleavage planes and grain boundaries occurred along the main fractures and at the side where the stress wave entered the sample (Figs. 5c, d). Such microstructures, coupled with the general absence of shear strain, are very similar in natural *in-situ* shattered dolostones (compare Figs. 5a, d with Figs. 1c-e).

4.2. FRACTURE PATTERN ANALYSIS

The three-dimensional fracture patterns of quasi-statically and dynamically deformed samples were quantified and compared by using image analysis applied to X-ray computed tomography datasets (for details see Supplementary Material) (Figs. 6a-c). To extract the

fracture network from the tomographic images we used the approach implemented by Voorn et al. (2013) (multiscale Hessian fracture filter – MSHFF) for the software FIJI (Schindelin et al., 2012), which was optimized for the enhancement and segmentation of narrow planar features such as fractures (see Supplementary Material). Further properties of the fracture network such as fracture intensity, bulk fracture orientation and aperture were determined after Voorn et al. (2015) using both FIJI and CTAn software (for details see Supplementary Material). The fracture skeletons were analyzed in two dimensions on slices oriented orthogonal to the loading direction.

Volumetric fracture intensity values (total fracture surface/sample volume) were significantly higher for dynamically shattered samples ($\sim 4.0 \text{ mm}^{-1}$) compared to quasi-statically fractured ones ($\sim 1.4 \text{ mm}^{-1}$) (Fig. 6b). Bulk fracture aperture followed a unimodal distribution (modal value $\sim 0.03 \text{ mm}$ for samples S4 and S26, Fig. 6c) in shattered samples while it was characterized by a polymodal distribution (modal values $> 0.1 \text{ mm}$ for sample U4, Fig. 6c) in quasi-statically fractured samples. In both cases fractures were oriented almost parallel to the loading direction (Fig. 6b). In terms of strike fractures generated under dynamic loading were quite scattered or arranged in a orthorhombic geometry (“low hierarchy” fracture pattern), while fractures produced under quasi-static loading were clustered around the orientation of few leading fractures (“high hierarchy” fracture pattern) (Figs. 6a, b). Overall the fracture patterns produced by dynamic loading were characterized by a much higher number of fracture branches and intersections compared to the quasi-static ones (Fig. 6d).

4.3. FRAGMENT SIZE DISTRIBUTIONS OF THE SHATTERED DOLOSTONES

Fragment size distributions (FSD) of experimental shattered dolostones were determined in two dimensions by manual drawing on X-ray tomographic images over an area of $\sim 0.8 \text{ cm}^2$ which was constrained by the dimensions of the experimental samples (for details see Supplementary Material). To allow a comparison, the FSDs of natural shattered dolostones (see Fig.1f) were recalculated on the same smaller analysis domains (area $\sim 0.8 \text{ cm}^2$) (Fig.7). The resulting FDSs of both natural and experimental shattered dolostones were comparable in the size range 0.01-4 mm with an average slope of 0.73 ± 0.14 in logarithmic plots (Fig.7). The slopes were computed in the narrower range of 0.1-1 mm where the curves had a linear trend (Fig.7), thus avoiding the external intervals which are affected by bias related to the spatial resolution of the images (data truncation) and to the finite size of the analysis domain (data censoring). Recalculated slopes (D) of natural shattered dolostones are smaller (~ 0.7 on average; Fig.7) than the ones determined on larger analysis domains (~ 1.2 on average; Fig.1f). The different slopes in the fragment distributions plots are certainly due to the undersampling effects associated to the reduction of the analysed sampled area. However, the diverse slopes might also suggest that the FSDs of these rocks are neither spatial heterogeneous nor self-similar. To investigate this hypothesis it would be necessary to determine the fragment size distributions over a much larger size range (i.e. three to four orders of magnitude).

5. DISCUSSION AND CONCLUSIONS

5.1. ENERGY SINKS AND DAMAGE

Experimental results indicate that intensely fragmented *in-situ* shattered dolostones were produced in compression when the applied critical strain rate was $> 120 \text{ s}^{-1}$ and the peak stress was on average larger than the uniaxial compressive strength of the rock (227.3 ± 45

MPa) (Figs. 4a-c). In particular, when we considered the strain energy dissipated in the sample up to the peak stress ($E_{diss-\sigma MAX}$ in Table 1), the occurrence of an energy threshold of ~ 1.8 MJ/m³, above which *in-situ* shattering start to develop, was evident (Fig.8). Interestingly this energy threshold was larger than the total energy dissipated in the pulverization of crystalline rocks such as quartz-monzonite (~ 1.5 MJ/m³; Aben et al., 2016a) and calcitic marble (~ 1.1 MJ/m³; Doan and Billi, 2011). Estimates of surface fracture energies for the shattered samples (E_s in Table 1) were 40-80% of dissipated strain energy (E_{diss} in Table 1, see Supplementary Material). The dynamically fragmented samples had distinctive characteristics compared to quasi-statically fractured ones: (i) higher fracture intensity, (ii) narrower fractures, (iii) low-hierarchy and high-complexity of the fracture pattern (Figs. 6a-d). All these characteristics are consistent with high strain rate loading during which the energy supply to the sample is too fast to be dissipated by only few fractures: this results in intense fragmentation of the rock (Grady and Kipp, 1989; Bhat et al., 2012; Doan and d'Hour, 2012, Aben et al, 2016b). On the other hand quasi-statically loaded samples displayed typical low-rate propagation features such as subaxial wing cracks growing at the tips of inclined fractures (e.g., Ashby and Sammis, 1990). Instead, the relatively abundance of curvilinear fractures in the outer portion of the samples was due to non-uniform stress distribution and lack of confinement during the tests (Peng and Johnson, 1972), and has to be considered as an artifact when compared with natural fault rocks. This was not the case for dynamically loaded samples, which were instead affected by radial fractures due to the occurrence of dynamic confinement (radial confinement up to ~ 0.5 MPa, see Supplementary Material) at high loading rates, when the effect of material inertia becomes significant (Doan and Gary, 2009; Chen, 2011).

5.2. IN-SITU SHATTERING: NATURE VS. LAB

In-situ shattered dolostones were exclusively produced at high dynamic loading rates in the laboratory. The deformation conditions determined for shattering in dolostones (critical strain rate $> 120 \text{ s}^{-1}$, axial strain $> 2\%$, Fig. 4) were comparable to those associated to pulverization of homogeneous crystalline rocks (i.e., granite, quartz-monzonite, calcitic marble; Doan and Gary, 2009; Yuan et al., 2011, Doan and Billi, 2011; Aben et al., 2016a) and considered to be transiently achieved in the fault wall rocks during the propagation of an earthquake rupture (e.g., Ben-Zion and Shi, 2005; Reches and Dewers, 2005). Moreover, in contrast to the quasi-statically deformed samples, experimentally shattered dolostones showed striking similarities with the natural ones of the Foiana Fault Zone: (i) two dimensional FSDs determined at the scale of the experimental samples (area $\sim 0.8 \text{ cm}^2$) were comparable (average slope = 0.73 ± 0.14 , size range = 0.01-4 mm) (Figs. 7), (ii) rock fragments were frequently exploded with no evidence of shear strain, (iii) pervasive extensional fracturing locally occurred down to the micrometer scale (microfragmentation domains) (Figs. 1c-e and Figs. 5a-d). All these observations suggest that also natural *in-situ* shattered dolostones had a dynamic origin potentially related to multiple off-fault coseismic stress-wave loadings (Fondriest et al., 2015).

5.3 SHATTERED DOLOSTONES AND HYDRAULIC DILATION BRECCIAS

The shattered dolostones of the Foiana Fault Zone are characterized by a well-fitted jigsaw puzzle texture which in most of the cases is comparable to that of the *crackle breccias* defined by Woodcock and Mort (2008) in their “non-genetic” fault breccias classification (more than 75% of sample area covered by clasts $> 2 \text{ mm}$ in size). This type of fault breccia was originally described in the dolomitic host rocks of the Dent Fault (northwest England) and

characterized by extensive infill of the fracture network by hydrothermal carbonate cement (Tarasewicz et al., 2005; Woodcock et al., 2006). In a similar way many *crackle* and *shatter* breccias described in the mining literature as fault-related were associated to hydraulic implosion mechanisms and frequently cemented by the deposition of hydrothermal minerals (e.g., Phillips, 1972; Mitcham, 1974; Sibson, 1986). According to Sibson (1986) implosive brecciation is a dynamic coseismic process generated by a sudden collapse of the wall rock at dilational fault jogs (mainly during rupture arrest) coupled with the generation of strong pore fluid pressure gradients. Compared to implosion hydraulic breccias, the shattered dolostones of the Foiana Fault Zone (i) were observed in different fault zone sections (straight fault segments and restraining bends; Fig. 1a) and, (ii) did not show presence of veins or cement filling the fracture network (see Fondriest et al., 2015 for details). Basing on the experimental results presented in this study (all the experiments were performed in “dry”- room humidity conditions, see section 3) *in-situ* shattered dolostones of the Foiana Fault Zone are the result of off-fault coseismic damage due to the propagation of multiple earthquake ruptures in a relative fluid-poor environment. This hypothesis might be furtherly reinforced by the occurrence of other structural features such as highly localized mirror-like fault surfaces lined by thin ultracataclastic layers, sharply truncating the shattered dolostones and previously interpreted as evidence of extreme coseismic shear strain localization based on field, microstructural and experimental observations (see for more details Fondriest et al., 2013, 2015).

5.4. IMPLICATIONS FOR SCALING RELATIONS IN FAULT ZONES

The experimental observations presented here open the possibility to reinterpret the origin of low-strain breccias (10-100s m thick) frequently associated with fault zones in

328 carbonates and classically interpreted in relation to the “slow” quasi-static growth of faults (i.e.,
329 nucleation and interaction of various generations of joints, pressure solution seams and shear
330 fractures; e.g., Salvini et al., 1999; Billi et al., 2003; Agosta et al., 2006). Many of these breccias,
331 especially within stiff dolomitic protoliths, might instead be produced by dynamic shattering
332 during the propagation of earthquake ruptures and then be more efficiently affected by
333 dissolution-precipitation and mass transfer processes during the post- or inter-seismic periods
334 (e.g., Gratier et al. 2014). Following this line of thought most of the volume of these fault zones
335 would be generated during earthquakes as it is also suggested by aftershocks spatial
336 distributions along active seismogenic faults (e.g., Valoroso et al., 2013). Moreover faults
337 associated with *in-situ* shattered fault rocks are frequently characterized by thickness vs.
338 displacement (t/d) ratios which are significantly higher (i.e., $t/d \sim 1$) compared to the classical
339 scaling relations estimated for relatively “simpler” fault zones (i.e., characterized by discrete
340 fault surfaces and well described by the “*damage zone-fault core*” model of Caine et al., 2010)
341 according to purely geometric quasi-static growth models ($t/d \sim 0.1$; e.g., Childs et al., 2009).
342 This is particularly evident within near-tip fault sections, as in the case of the southern sector of
343 the Foiana Fault Zone, where cumulative displacement tends to be low and the effects of slip
344 accumulation by stable sliding are likely to be minimized (Fig. 9). Therefore the occurrence of
345 high thickness vs. displacement ratios, coupled with the presence of *in-situ* shattered fault
346 rocks, can potentially be used to assess (i) the propagation of earthquake ruptures at shallow
347 depth along carbonate fault zones, and (ii) the hazard related to seismogenic sources with
348 incomplete earthquake catalogs. As a consequence the accurate mapping of the distribution of
349 *in-situ* shattered fault rocks along seismogenic fault zones and the precise quantification of

their fracture intensity represent the base for future robust evaluations of the actual contribution of surface fracture energy in the earthquake energy balance at shallow depth (i.e., < 3 km).

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Figure 1. Natural *in-situ* shattered fault rocks. (a) Aerial view of the central and southern sectors of the Foiana Fault Zone (Southern Alps, Italy; see inset on the top right): main fault strands colored in red. Actual and inferred exposures of *in-situ* shattered dolostones along fault strike were represented by blue areas; attitudes of the bedding around the fault were indicated with white symbols. Low-hemisphere projection stereoplots represent joints attitude (both as poles to planes and strike rose diagrams) moving from south (outcrop 1) to north (outcrop 2) along fault strike. Joints were mainly parallel and perpendicular to the average fault strike. (b) View of the Foiana Fault Zone (outcrop 1) exposed within a badland area. The exposed fault zone is > 300 m thick and consists of *in-situ* shattered rocks: intensely fragmented dolostones with little to no evidence of shear strain (see inset on the right). (c-e) Rock fragments of the *in-situ* shattered dolostones ranged from few centimeters down to few millimeters in size (c: hand specimen photograph; e: tracings of the clasts at the thin section scale) and (d) were locally

characterized by micro-fragmentation zones affected by penetrative extensional fracturing down to the micrometer scale. (f) Clast size distribution of *in-situ* shattered dolostones measured at the thin section scale (investigated area $\sim 5 \text{ cm}^2$) in directions both parallel and perpendicular to the fault strike. The two distributions had comparable slopes in the cumulative number (N) vs. equivalent diameter logarithmic plot.

Table 1. List of uniaxial compression tests of this study. High-strain rate uniaxial compression tests (#test: S1-S29) and low-strain rate uniaxial compression tests (#test: U1-U18). Symbols: d = sample diameter; L = sample length; σ_{MAX} = peak axial stress; UCS = uniaxial compressive strength; ϵ_{AMAX} = maximum axial strain; ϵ_{R} = residual axial strain; ϵ'_{MAX} = maximum strain rate; ϵ'_{A} = applied strain rate; ϵ'_{C} = critical strain rate; E_{KIN} = input kinetic energy; E_{diss} = dissipated strain energy; $E_{\text{diss-}\sigma\text{MAX}}$ = dissipated strain energy up to the peak stress; E_{S} = surface fracture energy; damage = sample damage state after the test. Damage: I = macroscopically intact; sp = split; SH = shattered; F = incipient and prominent fragmentation; f = sample faulted; sp+f = sample split and faulted. Indications: gages broken = strain gages broken during the test.

Figure 2. Low strain rate uniaxial compression tests. (a) Relation between uniaxial compressive strength (UCS) and length to diameter ratio of the Mendola Formation rock cylinders tested at strain rates of 6.7×10^{-6} and $6.7 \times 10^{-5} \text{ s}^{-1}$. UCS values were relatively scattered. In the photo, macroscopic Andersonian-oriented fracture of a sample at the end of experiment U12. (b) Thin section scan of the fractured sample U2 cut parallel to the loading direction (indicated by the vertical black arrow). The sample was affected by sub-axial extensional fractures (longitudinal

splitting) more densely concentrated in the outer portion of the sample. The internal portion of the sample U2 was affected by staircase arrays of oblique fractures (red in colour) and sub-axial wing-like cracks. (c) Thin section scan of the fractured sample U2 cut perpendicular to the loading direction. The sample was affected both by circular and radial extensional fractures in its outer portion and tiny closed shear fractures associated to shear comminution within the inner portion (see magnified SEM-BSE image in the inset).

Figure 3. High strain rate uniaxial compression tests. (a-c) Axial stress (blue in color line), axial strain (red line) and strain rate (green line) histories of dynamically loaded samples and associated damage states. σ_{MAX} and ϵ'_c indicate the peak axial stress and critical strain rate respectively, following the terminology of Table 1. Shattered samples (Fig. 3c) were characterized by a peculiar mechanical history compared to macroscopically intact and split ones, with a double-pick strain rate path. The relative strain rate minimum corresponds to the critical strain rate value for shattering in the test. (d) Stress vs. axial strain history of dynamically loaded samples. Macroscopically intact and split samples showed a quasi-elastic to anelastic behavior with residual strains <1%. Shattered samples accumulated residual strains always > 2%.

Figure 4. Deformation conditions for *in-situ* shattering. (a-c) Summary of high strain rate compression experiments. Samples were shattered over strain rates of $\sim 120 \text{ s}^{-1}$ if the applied peak stress was on average higher than the average UCS of the rock. Moreover experimentally

shattered samples showed a distinct clustering compared to the other samples in terms strain energy dissipation.

Figure 5. *In-situ* microstructures of experimentally shattered samples. (a) X-ray microtomography slice (sample S4) oriented perpendicular to the loading direction. Intense rock fragmentation with fine-grained material (down to the micrometer scale) lining main fractures is recognizable. Stress (blue line), strain (red line) and strain rate (green line) history of sample S4 is reported in the top left inset. (b) SEM-BSE images mosaic of the shattered sample S4 cut parallel to the loading direction (black in color arrow). Rock fragments were mostly few millimeters in size, elongated in the loading direction and delimited by sub-parallel extensional fractures. Pulverization (extensional fracturing down to the micrometer/crystal size scale) occurred along the main fractures (some of the infilling material was lost during sample polishing) and at the side where the stress wave entered the sample (see BSE-SEM magnified image in the inset). (c-d) SEM-BSE images with details of rock pulverization by crystal boundary breakage and fragmentation along cleavage planes.

Figure 6. Fracture pattern analysis. (a) X-ray tomography slices of the fracture pattern of a quasi-statically fractured sample (test U4) and a dynamically shattered one (test S26) enhanced by the application of a multiscale Hessian fracture filter (MSHFF) (Voorn et al., 2013). Since quasi-statically loaded samples were larger compared to dynamically shattered ones, which were even affected by dynamic confinement effects, both the entire (e.g., U4 in the figure) and inner-core (e.g. U4sub in the figure) fracture pattern of quasi-statically fractured samples were

compared with dynamically shattered ones. The yellow dashed circumference delimits U4sub which is comparable in size to sample S26 (the size comparison is highlighted by the two yellow dashed lines). (b) Three dimensional fractures orientation (poles to fracture planes; see Voorn et al., 2015). Quasi-statically fractured samples (test U4) were affected by few circular fractures and many Andersonian-oriented leading fractures (high hierarchy pattern). Dynamically shattered samples (test S26) were affected by many fractures with variable strike orientation and few leading ones (low hierarchy pattern). Volumetric fracture intensity was always larger for dynamically shattered samples compared to quasi-statically fractured ones. (c) Three dimensional fracture aperture distribution (number of voxel per aperture interval) was significantly different (polymodal vs. unimodal) for quasi-static fractured samples compared to dynamically shattered ones. (d) The two dimensional fracture skeleton of dynamically shattered samples was characterized by a higher number of fracture branches compared to quasi-statically fractured ones.

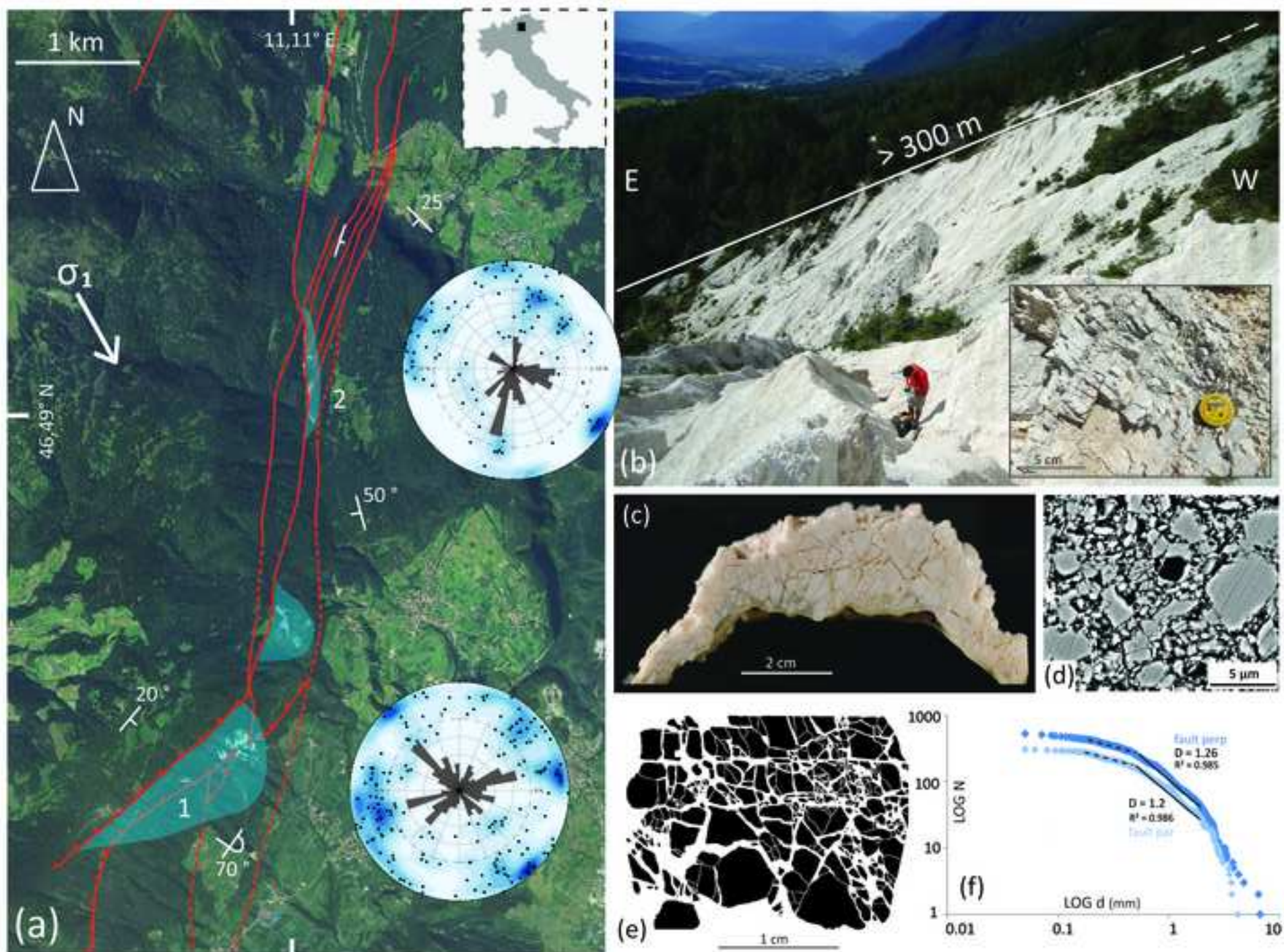
Figure 7. Two dimensional fragment size distribution of (i) natural *in-situ* shattered dolostones measured on sections oriented both parallel and perpendicular to the average strike of the Foiana Fault Zone, and (ii) experimental shattered dolostones measured on sections oriented perpendicular to the loading direction. The distributions of both natural and experimental samples were comparable (i.e. similar slopes), thus suggesting a common dynamic origin for these shattered rocks. The clast size distributions were measured on equivalent surfaces of 0.78 cm^2 which was constrained by the dimension of the experimental samples.

Figure 8. Plot of dissipated strain energy up to the peak stress vs. maximum axial strain. Experimentally shattered samples were characterized by much higher axial strains and slightly higher strain energies dissipated up to the peak stress compared to the quasi-statically fractured ones. Peculiarly shattered samples were produced only when an energy threshold of $\sim 1.8 \text{ MJ/m}^3$ was overcome, which was significantly higher compared to the energy dissipated by quasi-static compressive fracturing.

Figure 9. Fault rocks thickness vs. cumulative fault displacement scaling relations after Childs et al. (2009) for various host rocks and fault kinematics (a,b). *In-situ* shattered dolostones at the southern portion of the Foiana Fault Zone (displacement = 0.3-0.5 km, outcrop 1 in Fig.1a) were > 300 m thick and lied out of the scaling trend displayed in the plots which are associated to quasi-static fault growth models. Moving to the north (outcrop 2 in Fig.1a) the cumulative displacement increased up to 1.6-1.8 km and the thickness of shattered rocks was $\sim 100 \text{ m}$. Here the scaling relation was more consistent with the one proposed by Childs et al. (2009).

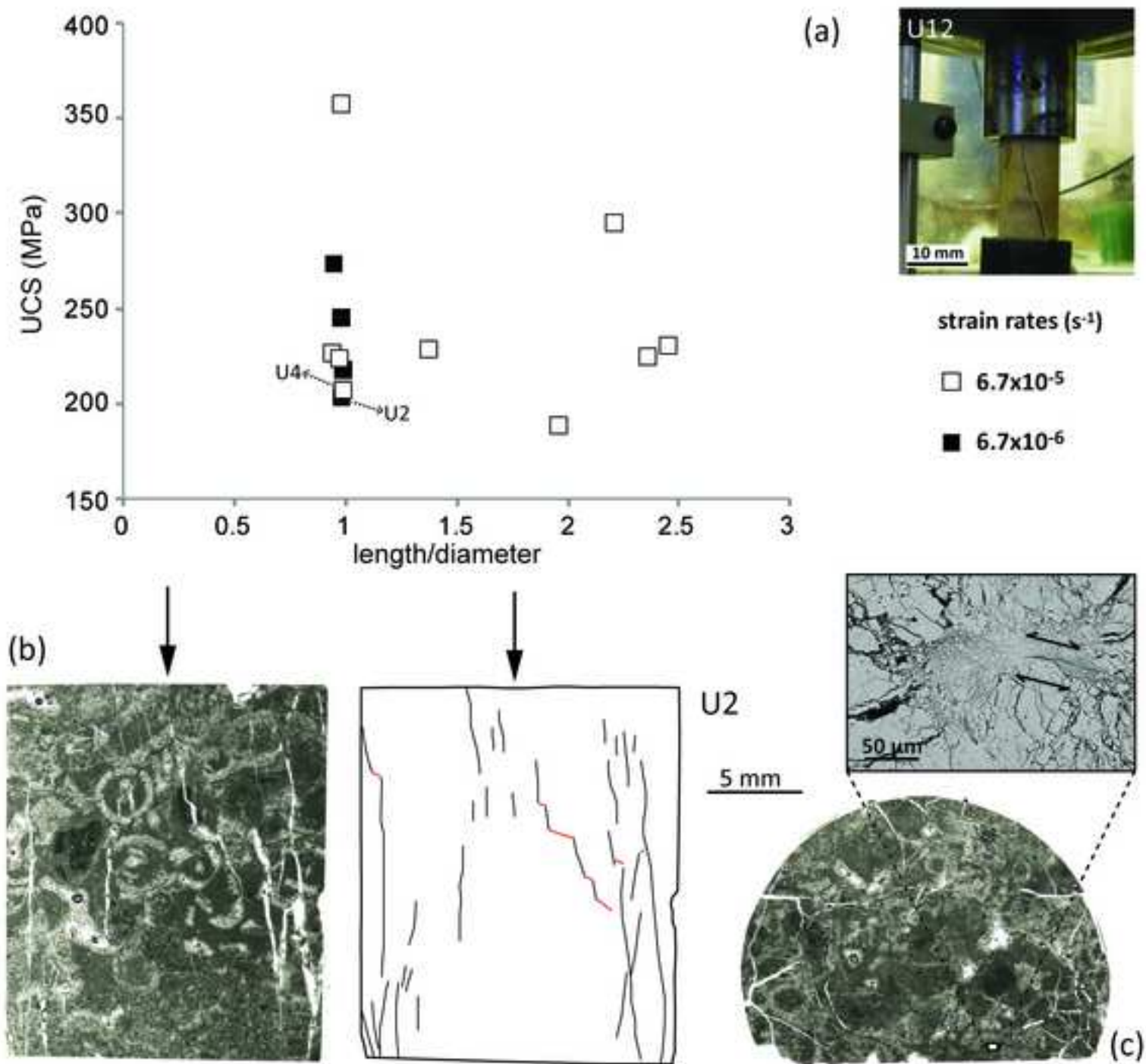
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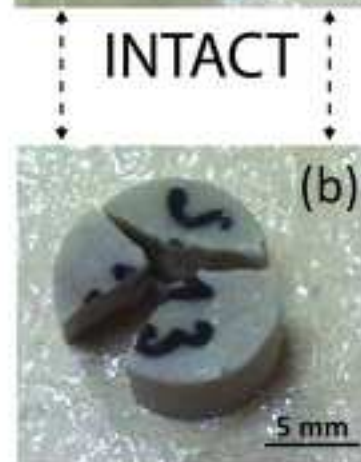
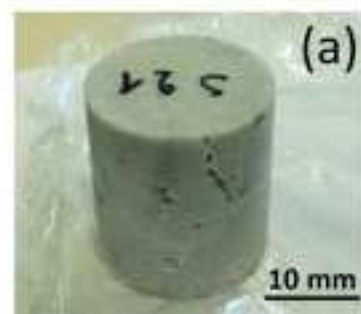
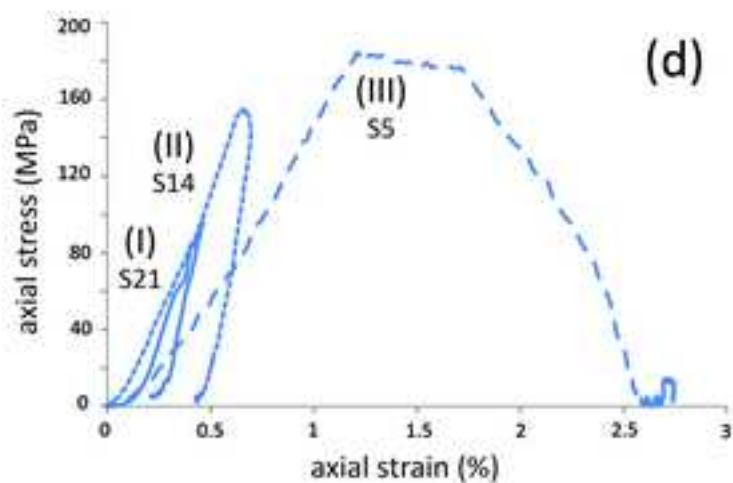
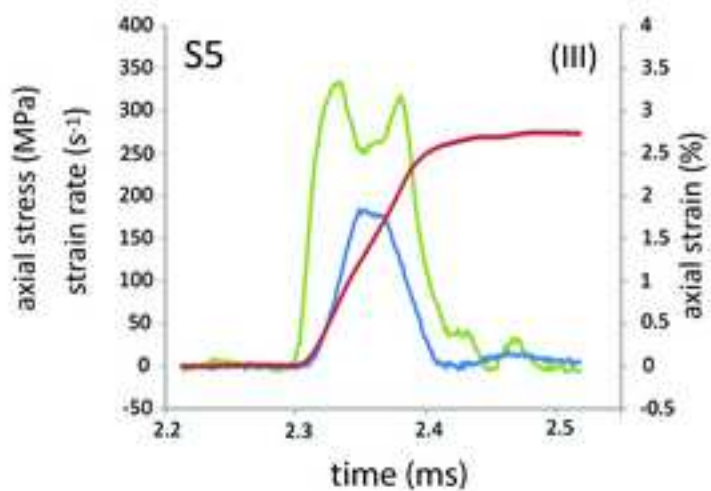
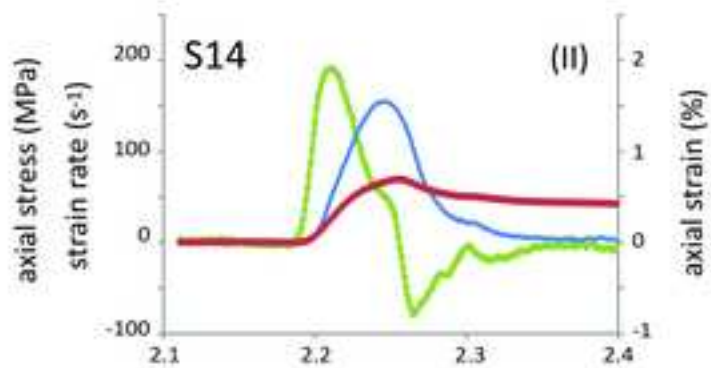
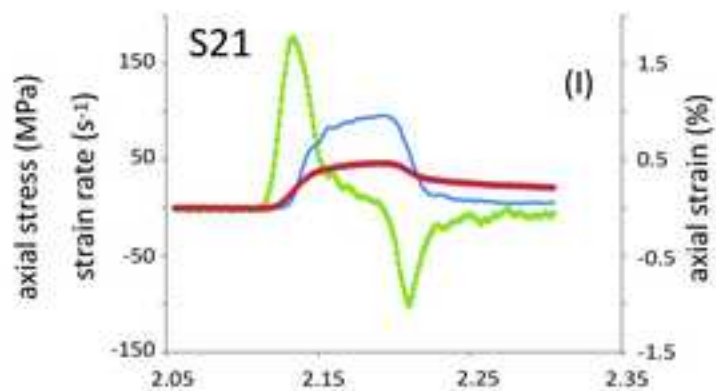
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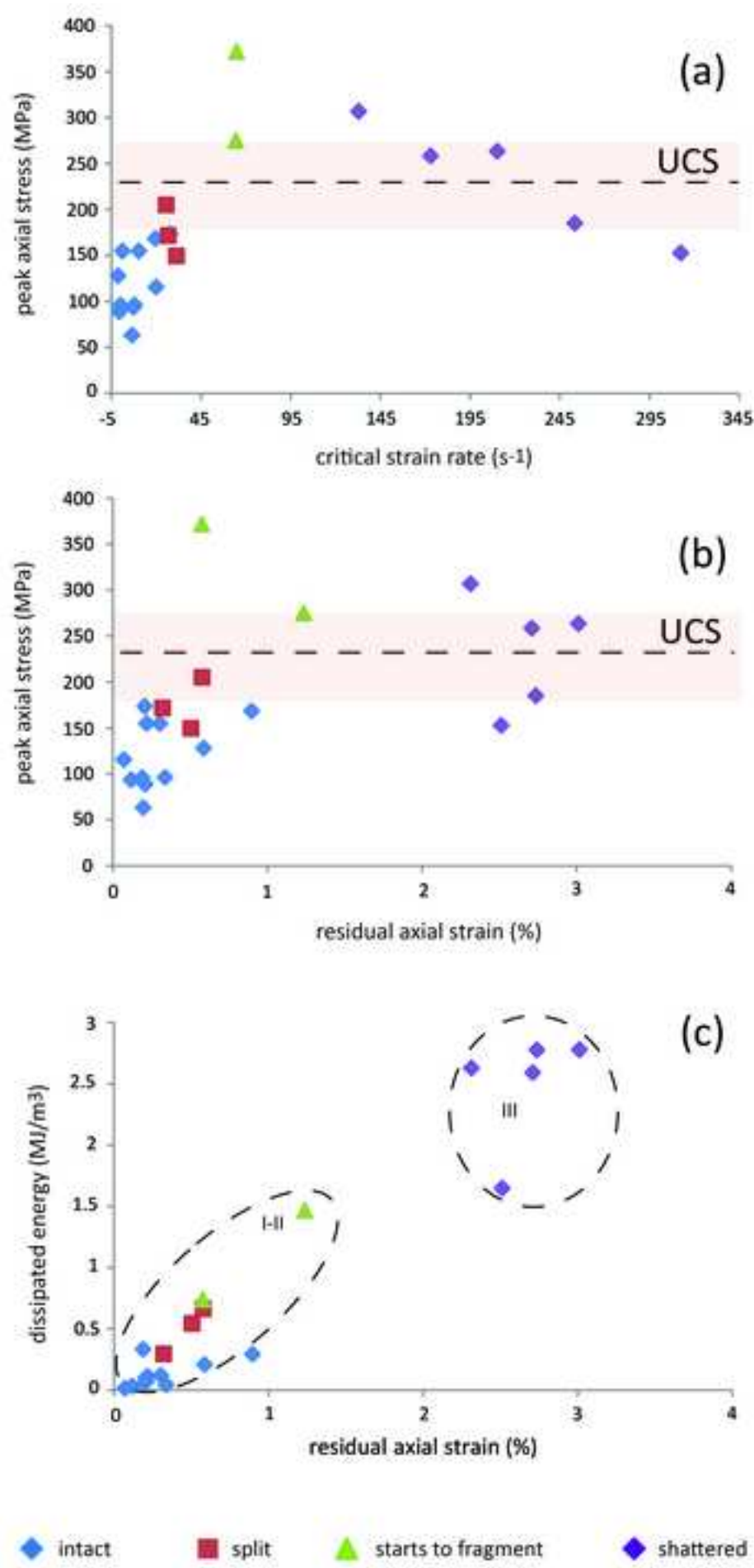
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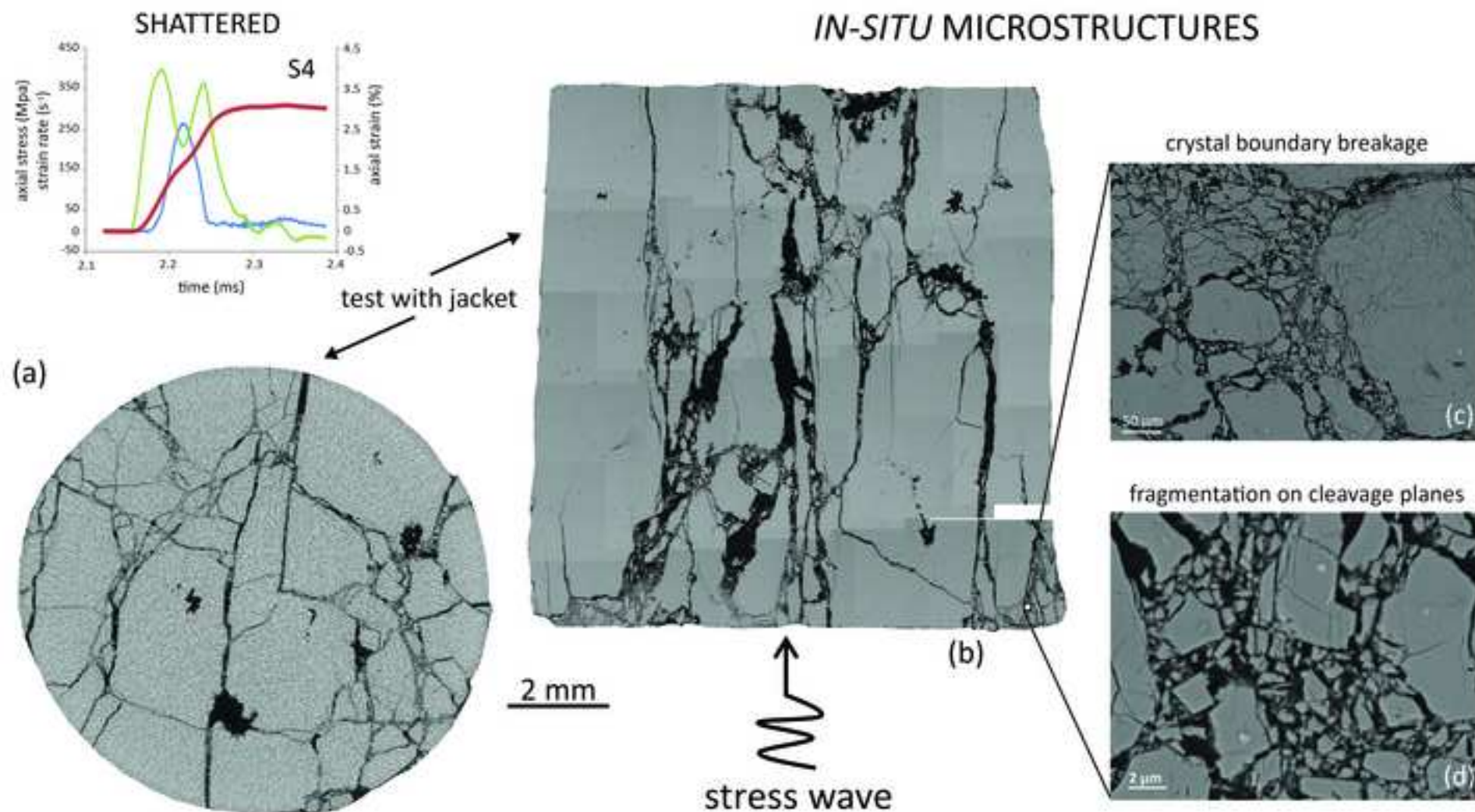
— strain rate (s^{-1})
— axial strain
— axial stress (MPa)

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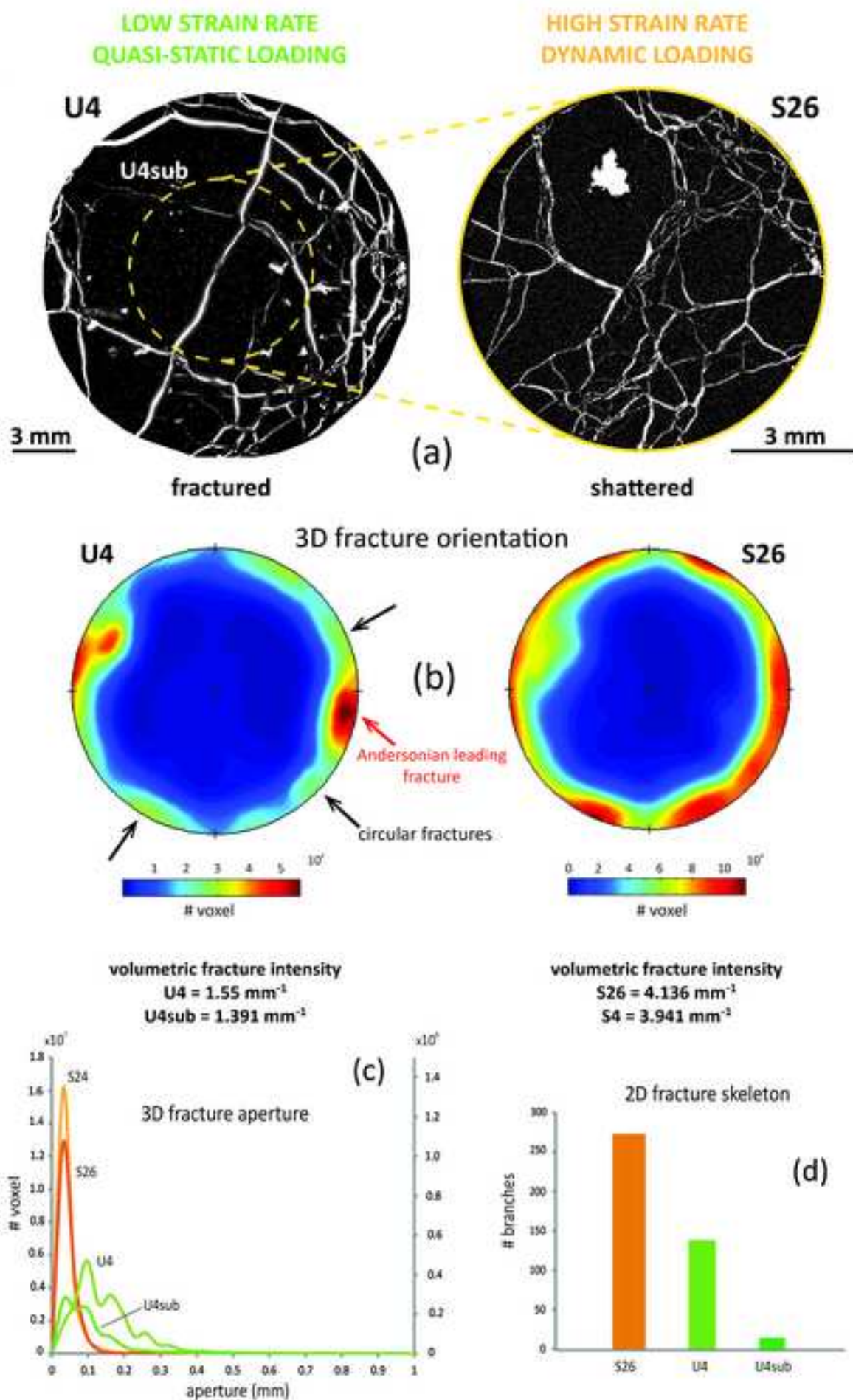
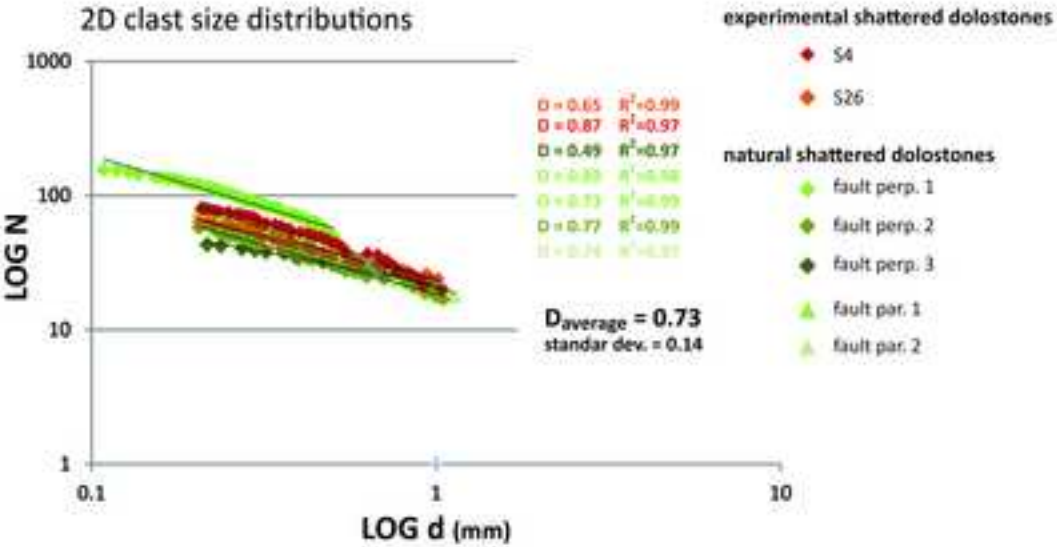
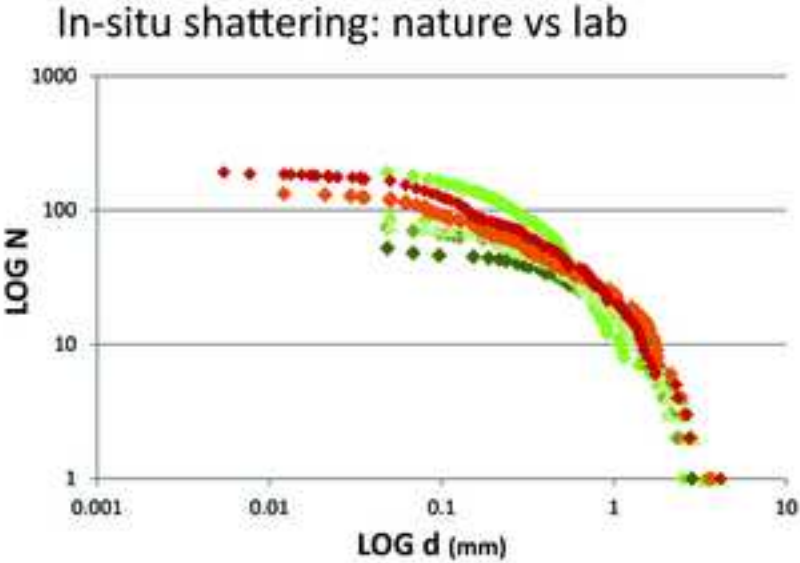


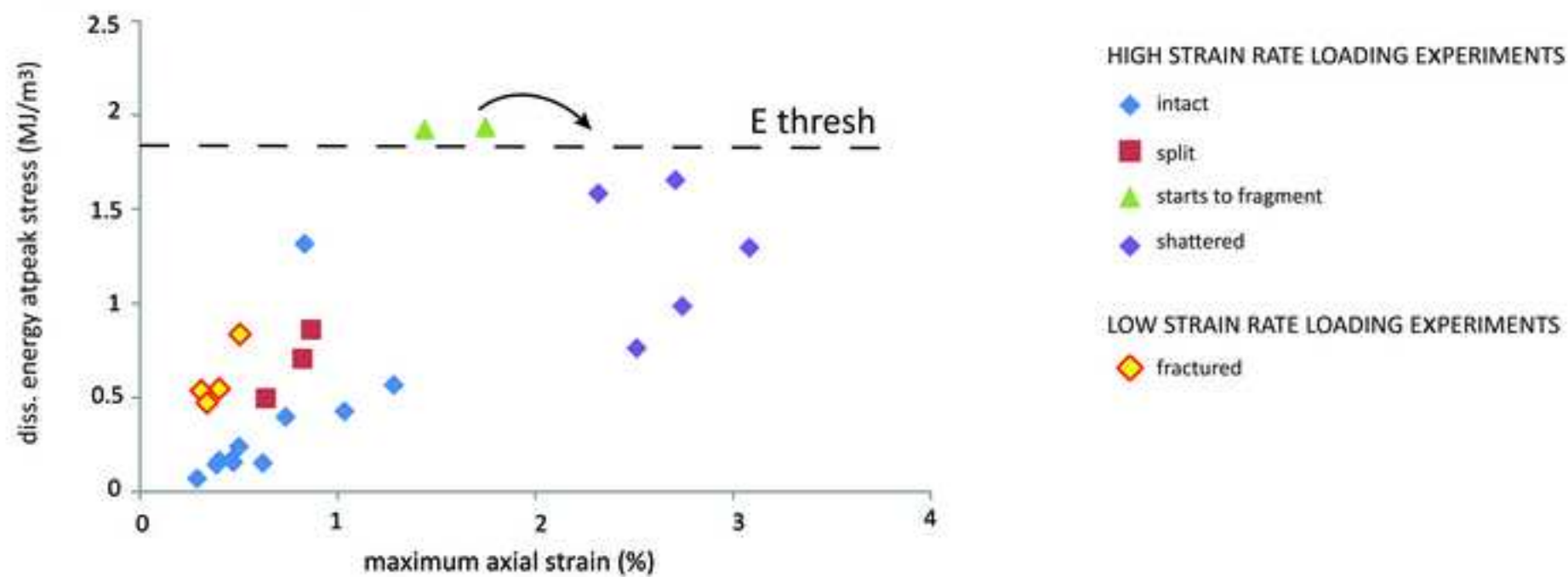
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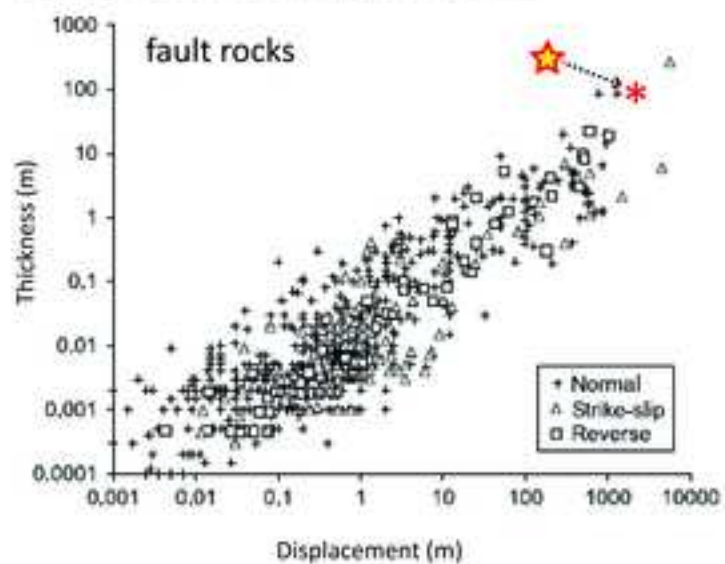
Energy sinks and damage



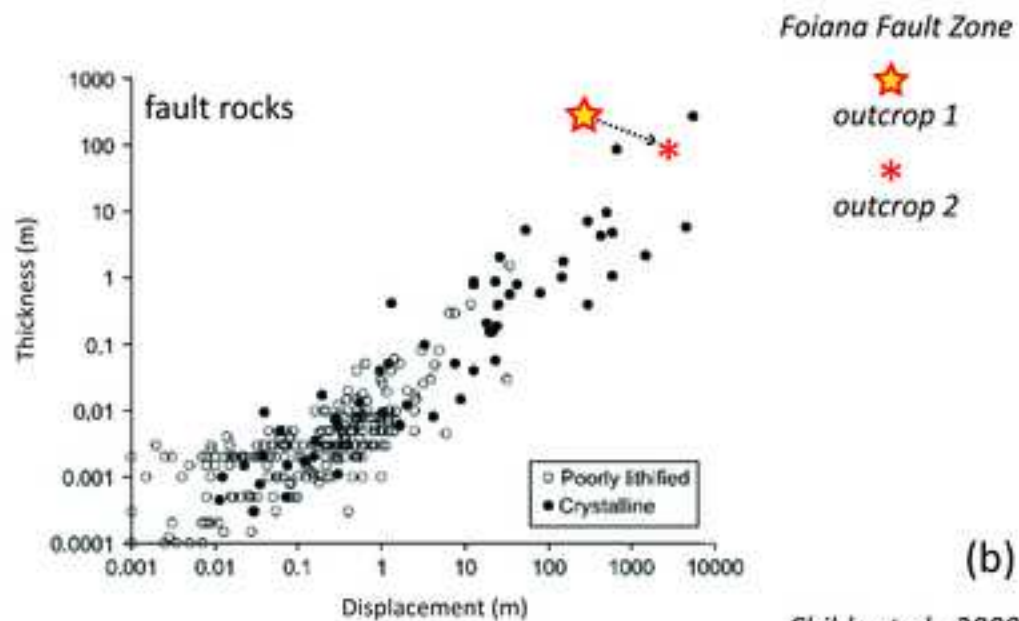
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Fault zones scaling relations



(a)



(b)

Childs et al., 2009

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Table
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# test	d (mm)	L (mm)	σ_{MAX} (Mpa)	ϵ_{AMAX} (%)	ϵ_R (%)	ϵ'_{MAX} (s ⁻¹)	ϵ'_c (s ⁻¹)	E_{LIN} (MJ)	E_{DISS} (MJ/m ³)	$E_{DISS-\sigma MAX}$ (MJ/m ³)	E_s (MJ/m ³)	damage
S1	15.0	15.0	168.3	1.3	0.9	312.8	19.6	6.5	0.29	0.56	-	I
S2	15.0	14.9	171.7	0.6	0.3	185.7	26.7	0.0	0.30	0.49	-	sp
S3	15.0	14.8	149.5	0.8	0.5	144.7	31.3	0.0	0.54	0.71	-	sp
S4	9.6	9.4	263.3	3.1	3.0	397.2	210.2	6.7	2.78	1.29	1.18	SH
S5	9.8	9.2	185.0	2.7	2.7	334.8	253.4	5.5	2.78	0.98	-	SH
S6	-	-	-	-	-	-	-	-	-	-	-	F
S7	9.6	9.5	275.0	1.7	1.2	306.1	64.9	5.6	1.47	1.93	-	I
S8	9.4	9.6	258.3	2.7	2.7	313.1	173.0	6.2	2.59	1.65	-	F
S9	9.6	9.5	-	-	-	-	-	-	-	-	-	I
S10	9.6	9.7	152.7	2.5	2.5	415.8	312.5	4.7	1.65	0.76	-	SH
S11	9.6	9.2	371.7	1.4	0.6	449.3	64.5	5.0	0.74	1.92	-	I
S12	9.6	9.5	127.8	1.0	0.6	293.7	-1.3	1.5	0.21	0.42	-	F
S13	9.6	9.3	205.0	0.9	0.6	237.6	25.7	2.0	0.66	0.86	-	sp
S14	14.9	14.5	154.7	0.7	0.4	191.2	47.4	5.0	0.38	0.49	-	sp
S15	15.0	15.0	173.3	0.7	0.3	209.2	1.3	5.4	0.12	0.40	-	I
S16	14.9	14.8	115.7	0.5	0.2	180.7	10.4	2.2	0.11	0.24	-	I
S17	14.9	14.7	-	-	-	-	-	-	-	-	-	I
S18	14.9	15.0	88.7	0.4	0.2	143.9	27.9	1.5	0.10	0.16	-	I
S19	20.9	20.4	63.3	0.3	0.1	161.2	19.9	2.3	0.01	0.07	-	I
S20	20.9	20.5	-	-	-	-	-	-	-	-	-	I
S21	20.9	20.8	96.2	0.5	0.2	177.0	-0.5	7.1	0.07	0.17	-	I
S22	20.9	20.4	93.5	0.5	0.2	187.1	6.7	6.9	0.06	0.15	-	I
S23	-	-	-	-	-	-	-	-	-	-	-	I
S24	20.9	20.9	95.8	0.6	0.3	204.9	8.0	5.7	0.04	0.15	-	I
S25	20.9	21.0	96.7	0.4	0.1	168.7	7.4	5.8	0.03	0.14	-	I
S26	9.6	9.6	306.7	2.3	2.3	446.3	132.9	5.9	2.63	1.58	1.24	SH
S27	9.6	9.2	-	-	-	-	-	-	-	-	-	SH
S28	9.6	9.7	355.0	0.8	0.2	174.1	0.1	5.5	0.33	1.31	-	I
S29	9.6	9.5	335.1	1.0	0.6	173.3	41.9	0.0	1.36	2.81	-	F

# test	d (mm)	L (mm)	UCS (MPa)	ϵ_{AMAX} (%)	X	ϵ'_A (s ⁻¹)	X	X	X	$E_{DISS-\sigma MAX}$ (MJ/m ³)	E_s (MJ/m ³)	damage
U1	21.0	20.6	245.3	0.5	-	6.7x10 ⁻⁶	-	-	-	0.84	-	sp + f
U2	20.8	20.5	203.0	0.4	-	6.7x10 ⁻⁶	-	-	-	0.55	-	sp
U3	20.9	19.9	273.1	0.3	-	6.7x10 ⁻⁶	-	-	-	0.54	-	sp
U4	20.9	20.7	206.7	0.3	-	6.7x10 ⁻⁶	-	-	-	0.47	0.47	sp + f
U6	20.9	20.7	217.3	gages broken		6.7x10 ⁻⁶	-	-	-	-	-	sp
U8	21.0	20.7	206.9	gages broken		6.7x10 ⁻⁶	-	-	-	-	-	sp
U9	24.4	59.9	229.7	-	-	6.7x10 ⁻⁵	-	-	-	-	-	sp
U10	24.4	57.7	224.1	0.3	-	6.7x10 ⁻⁵	-	-	-	0.36	-	sp
U11	24.8	54.8	294.6	0.5	-	6.7x10 ⁻⁵	-	-	-	0.61	-	sp
U12	24.3	41.7	-	-	-	6.7x10 ⁻⁵	-	-	-	-	-	f
U13	24.4	47.7	188.4	0.5	-	6.7x10 ⁻⁵	-	-	-	0.37	-	sp
U14	24.4	33.4	227.7	0.5	-	6.7x10 ⁻⁵	-	-	-	0.52	-	sp
U15	24.3	24.0	206.8	0.4	-	6.7x10 ⁻⁵	-	-	-	0.47	-	sp + f
U16	24.4	22.9	226.1	0.7	-	6.7x10 ⁻⁵	-	-	-	1.04	-	sp
U17	20.8	20.3	222.9	-	-	6.7x10 ⁻⁵	-	-	-	-	-	sp
U18	20.9	20.5	357.5	0.7	-	6.7x10 ⁻⁵	-	-	-	0.81	-	sp

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